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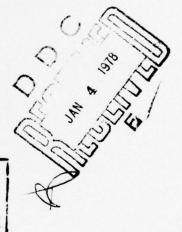
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TRANSONIC WIND TUNNEL TESTS ON A 1/8TH SCALE MK82 BOMB MODEL

B.D. FAIRLIE, L.J. ROBERTS AND R.G. BROADBENT

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TRANSONIC WIND TUNNEL TESTS ON A 1/8TH SCALE MK82 BOMB MODEL.

BY

B.D. FAIRLIE, L.J./ROBERTS R.G./BROADBENT

#### SUMMARY

Transonic wind tunnel tests have been conducted on a 1/8th scale model of a Mk82 bomb. The tests covered an incidence range of -2° to 28° and a Mach number range of 0.95 to 1.20 for roll angles between -45° and + 45°. The tests indicated that model exhibited static longitudinal stability for all condition except at low Mach numbers and incidences greater than about 20°.



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# NOTATION

$c_{D}$	Drag force coefficient = Drag force/2p V2S
c <sub>N</sub>	Normal force coefficient
	=Normal force/½p V2S
c <sub>X</sub>	Axial force coefficient
	= Axial force/ $\frac{1}{2}$ $^{\circ}$ $V^{2}$ S
CXB	Base force coefficient
	$= (P_{b-P}) s_B / P_V^2 s$
CY	Side force coefficient
	= Side force/ $\frac{1}{2}\rho$ V <sup>2</sup> S
Cl	Rolling moment coefficient
	= Rolling moment/2 0 V2Sd
C <sub>m</sub>	Pitching moment coefficient
	= Pitching moment/2 p V <sup>2</sup> Sd
Cn	Yawing moment coefficient
	= Yawing moment/ $\frac{1}{2}$ $^{\rho}$ $V^2$ Sd
đ	Body diameter = 34.14 mm (1.344in)
M	Free stream Mach number
P	Free stream static pressure
$P_{\overline{B}}$	Model base pressure
R	Reynolds' number based on body diameter
S	Body cross sectional area = $915.5 \text{ mm}^2 (1.419 \text{in}^2)$
$s_B$	Model base area = $107.1 \text{ mm}^2 (0.166 \text{ in}^2)$
٧	Free stream velocity
ρ	Free stream density
0	Angle of incidence
. Ø	Model roll angle( $\emptyset=0$ - suspension point screws uppermost)

- Note: 1. See Fig. 1 for sign conventions for forces and moments.
  - 2. Nominal centre of gravity located 125.42mm (4.938in) from the nose.

#### INTRODUCTION

At the request of the Weapons Research and Development Wing of the Weapons Research Establishment a series of transonic wind tunnel tests were carried out on a 1/8th scale model of a Mk82 bomb. These tests were conducted in support of the research project "Store Separation from Aircraft" being pursued by the Weapons Research Establishment. To avoid the construction of a new model for these tests, an existing model and balance were supplied by W.R.E. This model had been tested at subsonic and higher supersonic speeds at W.R.E. and the tests reported here were required to investigate the longitudinal and lateral stability of the bomb in the transonic and low supersonic speed range.

The tests reported herein were conducted in the Aeronautical Research Laboratories' transonic wind tunnel during December 1976.

#### 2. TEST DETAILS

#### 2.1 Model

A dimensioned sketch of the 1/8th scale model of the Mk82 bomb is presented in Figure 2. Transition was fixed on the body by a row of discrete roughness spheres. The six component sting mounted strain gauge balance supplied with the model by W.R.E. was used for all tests.

#### 2.2 Wind Tunnel

All tests were conducted in the A.R.L. transonic wind tunnel. The nominal dimensions of the tunnel test section are 813mm by 533mm. For these tests the test section walls were all longitudinally slotted (Fig. 3) with an open area ratio at the model location of 10.5%.

The maximum frontal cross-sectional area of the model at zero incidence was 915mm<sup>2</sup> giving a blockage ratio of 0.21%. No corrections for the effects of tunnel interference were applied to the results.

Mach number and dynamic pressure were derived from measurements of the static pressure in the plenum chamber surrounding the test section and of the static pressure in the contraction entry, assuming these to be the static and total pressures respectively of the test section flow.

#### 2.3 Test Programme

Six component force and moment coefficients were measured over an incidence range of  $-2^{\circ}$ < 0 < 28° in 2° increments, for roll angles in the range  $-45^{\circ}$ < 0 <  $45^{\circ}$  in  $72^{\circ}$  increments. Model attitude was corrected for sting and balance deflections under load. The range of Mach number covered for each attitude was 0.95 < M < 1.20 in increments of 0.05. In addition, several runs were conducted at zero roll angle and various incidences with fine increments in Mach number to investigate the detailed form of variations with Mach number in the region where shock reflections were apparent.

The variation of test Reynolds number (based on body diameter) with Mach number is presented in Figure 4.

#### 3. RESULTS AND DISCUSSION

Complete results from the present tests are presented in Table I (See Fig. 1 for sign conventions).

Figures 5 and 6 show the variation of normal force coefficient and pitching moment coefficient with angle of incidence for selected representative roll angles ( $\emptyset = -45^{\circ}$ ,  $-22.5^{\circ}$ , 0°,  $+22.5^{\circ}$ ,  $+45^{\circ}$ ). The results show static longitudinal stability under all conditions except at lower Mach numbers and angles of incidence greater than about 20° where some instability is evident.

It was expected that the model would be subject to shock wave reflection interference over a range of supersonic Mach numbers. Since Schlieren observations of the flow in this test section were not possible, an estimate was made of the Mach number range for which this would be the case. The estimate was based on the assumption that wave reflection interference would commence at the Mach number for which a wave from the body shoulder was reflected back to the fin leading edge, and would continue with increasing Mach number until the nose shock reflection fell downstream of the model base. Reflection at the free stream Mach number was assumed, and the position of the nose shock was estimated by Moeckel's 1 geometric method. As shown in Fig. 7 the estimated Mach number range for the model at zero incidence was from 1.01 to 1.07.

Figure 8 shows the variation of pitching moment coefficient with Mach number for the fine Mach number increment, extended Mach number range runs. It is evident that wave reflection interference is present for Mach numbers in the range 1.00 M 1.08; in good agreement with the estimate.

The variation of rolling moment coefficient with angle of incidence is shown in Fig. 9 for M=0.95 & 1.20 and selected roll angles. The results for these Mach numbers were chosen since they should be free of interference effects and are representative of all the other tests. Fig. 9 shows a positive rolling moment at zero angle of attack of approximately 0.02 which remains constant under all conditions and can be attributed to the 120 cant of the fins. The behaviour of the rolling moment curves are typical of all fin stabilised stores when the fins are not symmetrically disposed about the plane of angle of incidence. When the angle of incidence exceeds about 10°, the fins on the leeward side of the body are influenced appreciably by non uniformity of the flow separating from the body. As the angle of incidence increases beyond 10° this influence becomes very marked and, at some roll angles, results in the annulment of the rolling moment due to fin cant. The effect of fin cant is also seen in the asymmetry of the effects of roll angle.

Similar plots of the variation of yawing moment and side force coefficients are shown in Figs. 10 and 11. Similar remarks to those made for the previous figure are also relevant to the variation with angle of incidence in both these cases.

#### 4. CONCLUSIONS

Transonic wind tunnel tests of a 1/8th scale model of a MK82 bomb have indicated that the model exhibits static longitudinal stability throughout the range of attitudes (-20 \leq 0 \leq 280; -450 \leq 6 \leq 450) and Mach numbers (0.95 \leq M \leq 1.20) covered in these tests. The model exhibits a variation of rolling moment at high angles of incidence which is typical of stores on which the fins are not symmetrically disposed about the incidence plane. The influence of roll angle on rolling moment is sufficient at some roll angles to overcome the rolling moment due to fin cant.

#### REFERENCES

# Author

1. Moeckel, W.E. Approxima

Title

Approximate Method for Predicting Form and Location of Detached Shock Waves Ahead of Plane or Axially Symmetric Bodies.
N.A.C.A. TN 1921, 1949.

# NOTATION FOR TABLE I

The following notation refers to the computer generated data listings of TABLE I. Where appropriate, the corresponding notation from the main body of the memorandum is also included.

TABLE I NOTATION	MAIN BODY NOTATION	EXPLANATION
SER	-	Serial number
REYN	R	Reynolds number
MACH	M	Mach number
THETA	θ	Angle of Incidence
RANG	Ø	Roll Angle
NORMAL	$c_N$	Normal force coefficient
PITCH	Cm	Pitching moment coefficient
AXIAL	$c_X$	Axial force coefficient
BASE	CXB	Base force coefficient
DRAG	$c_{\mathcal{D}}$	Drag force co- efficient
SIDE F	СҮ	Side force coefficient
YAW M	$c_n$	Yawing moment coefficient
ROLL M	c <sub>1</sub> .	Rolling moment coefficient

TABLE 1.01 DATA LISTINGS

ROLL ANGLE = -45 DEG.

								0421				
SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
17	0.150	0.949	-2.01	-45.0	0.1063	0.2738	-0.1525	0.0101	0.1662	-0.0037	0.0222	0.0181
	0.154		-2.01	-45.0	0.1176		-0,1798	0.0064		-0.0088	0.0366	0.0189
-	0.157	200000000000000000000000000000000000000	-2.02	-45.0	0.1030		-0.3129			-0.0076	0.0452	0.0179
-	0.160		-2.02	-45.0	2.1132		-0.3561			-0.0025	0.0122	0.0191
	0.163		-2.02	-45.0	0.1236		-0,3485			0.0042		0.0187
	0.167		-2.02		0.1486		-0,3614			-0.0111	0.0424	0.0190
	0.150		-0.01			-0.0544		0.0064		-0.0056	0.0226	0.0186
	0.154		-0.01			-0.0653		0.0063		-0.0107	0.0385	0.0187
-	0.157		-0.01			-0.0554		0.0147		-0.0103	0.0387	0.0168
26	0.162	1.098	-0.01	-45.0	-0.03/1	-0.102/	-0,3639	-0.0052	0.3580	0.0049	0.0052	0.0189
27	0.163	1.151	-0.01	-45.0	-0.0237	-0.0750	-0,3542	-0.0091	0.3450	0.0036	-0.0250	0.0186
	0.167		-0.01				-0,3714			-0.0110	0.0414	0.0188
	0.147		2.01			-0.1989		0.0070		-0,0128	0.0460	0.0195
30	0.154	0.999	2.01	-45.0	-0.1750	-0.2483	-0,1946	0.0066	0.2072	-0.0108	0.0411	0.0198
	0.157		2.02	-45.0	-0.1665	-0.1870	-0,3204	0.0120	0,3380	-0.0131	0.0686	0.0186
	0.160		5.05.				-0,3613			-0.0067	0.0190	0.0199
-	0.163	-	2.01				-0,3487			0.0023		0.0206
	0.167		2.02				-0,3704		The state of the s	-0.0173	0.0777	0.0197
	0.150		4.03			-0.3459		0.0056		-0.0068	0.0315	0.0213
36	0.154	1.001	4.03	-45,0	-0.3333	-0.4254	-0,1938	0.0046	0.2212	-0.0122	0.0375	0.0216
37	0.160	1.050	4.03	-45.0	-0.5122	-0.2791	-0.3057	0.0125	0.3392	-0.0149	0.0631	0.0200
	0.160		4.03				-0.3564			-0.0055	0.0133	0.0214
	Ø.183		4.03				-0,3530			-0.0069		0.0220
40	0.168	1.199	4.03				-0,3734			-0.0224	0.0991	0.0203
43	0.145	0.947	6.02	-45.0	-0.4573	-0.5085	-0,1502	0.0069	0.2042	-0.0097	0.0131	0.0247
										_		
	0.149		6.02				-0.1835			-0.0015		0.0244
	0.155		6.04			-0.4615		0.0110		-0.0203	0.0610	0.0240
	0.158		6.04				-0,3605			-0.0070	0.0259	0.0246
	0.162		6.04				-0,3430 -0,3644			-0.0008 -0.0289	0.1066	0.0256
40	0.102	1.200	0.04	-45,0	-0.4//6	-6.4201	-6,3044	-818883	0,403/	-0.0259	0.1000	0.0220
49	0.147	0.951	8.04	-45.0	-0.6252	-0.6923	-0.1576	0.0039	0.2473	-0.0059	0.0047	0.0275
	0.152		8.04			-0.7599		0.0027		-0.0132		0.0275
51	0.155	1.050	8.05	-45.0	-0.5480	-0.6086	-0.3131	0.0109	0.4115	-0.0194	0.2786	0.0278
52	0.158	1.100	8.05	-45.0	-0.6770	-0.7611	-0,3678	-0.0062	0,4527	-0.0100	0.0479	0.0291
53	0.162	1.150	8.05	-45. W	-0.6711	-0.7302	-0,3543	-0.0124	0.4324	0.0035	-0.0448	0.0288
						0 5	-0.7070					0.0015
	0.163		8.06				-0,3878			-0.0301	0.1366	0.0263
	0.147		10.05			-0.8891		0.0039		-0.0013	0.0184	0.0306
200	0.152		10.05			-0.9878 -0.8044		0.0037		-0.0127	0.0412	0.0317
	Ø.155 Ø.158		10.07				-0,3676			-0.0130 -0.0033	0.0508	0.0311
90	0.130	1,077	10.00	49,0	-0.056/	-0.7301	0,30/0	010000	0.0035	0.0033	0.0500	0.0324
59	0,162	1.148	10.07	-45.0	-0.8759	-0.9332	-0,3706	-0.0153	0.5029	-0.0001	-0.0065	0.0309

TABLE 1.01

#### ROLL ANGLE = -45 DEG.

SER	REYN MAC	H THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
60	0.163 1.19	10.08	-45.0 -2.849	-0 7139	-0.3898	-0.0133	0.5192	-0.0284	0.1401	0.0292
	0.147 0.94		-45.0 -1.0079			0.0042		-0.0035	0.0091	0.0298
	0.152 0.99		-45.0 -1.065			0.0013		0.0015	0.0202	0.0298
	0.155 1.04		-45.0 -1.0466			0.0098	CO. M	-0.0076	0.0321	0.7288
	0.160 1.10		-45.0 -1.081					-0.0073	0.3496	0.0315
04	D.100 1.10	12.07					,,,,,,,,	D. D. D. T. S	0.0470	
	0.162 1.14		-45.0 -1.098				0.5800		-0.0240	0.0306
	0.163 1.20		-45.0 -1.061	and the same of th				-0.0324		0.0289
69	0.144 0.95	14.08	-45.6 -1.226			0.0051	0.4326		-0.2776	0.0213
70	0.145 1.00	1 14.08	-45.0 -1.285			0.0000		-0.0017		0.0223
71	0.152 1.05	14.09	-45.0 -1.313	7 -1.2864	-0,3378	0.0099	0.6572	0.0156	-0.0107	0.0208
72	0.154 1.10	1 14.09	-45.0 -1.311	-1.3328	-0,3721	-0.0102	0.6705	0.0086	-0.3029	0.0268
73	0.157 1.14	9 14.11	-45.0 -1.526	2 -1.2698	-0,3770	-0.0167	0.6727	0.0140	-0.0728	0.0235
74	0.160 1.20:	1 14.13	-45.0 -1.304	3 -1.0051	-0,3950	-0.0147	0.6872	-0.0106	0.0987	0.0224
75	0.145 0.94	16.09	-45. V -1.465	7 -1.5809	-0,1277	-0.0026	0.5263	0.0328	-0.1034	0.0114
	0.149 1.00		-45.0 -1.545	3 -1.6526	-0,1707	-0.0004	0.5922	0.0464	-0.1122	0.0121
77	0.150 1.05	16.14	-45.4 -1.001	3 -1.1615	-0,3094	0.0055	0.7198	0.0462	-0.1037	0.0095
78	0.154 1.10	16.12	-45.0 -1.556	3 -1.4524	-0,3767	-0.0138	0.7810	0.0374	-0.0536	0.0213
79	0.158 1.15	1 16.15	-45.0 -1.276	7 ~1.3806	-0,3705	-0.0192	0.7757	0.0458	-0.1329	0.0175
80	0.160 1.19	16.17	-45.6 -1.564	5 -1.0397	-0.3950	-0.0163	0.7993	-0.0046	0.0755	0.0131
81	0.145 0.94	8 18.11	-45.0 -1.728	3 ~1.8622	-0,1384	-0.0037	0,6652	0.0482	-0.1131	0.0112
82	Ø.149 Ø.99	7 18.13	-45.6 -1.8396	-1.9455	-0.1522	-0.0055	0.7117	0.0711	-0.2059	0.0082
	0.152 1.05		-45.0 -1.857		The state of the s		0.9057	0.0871	-0.2671	0.0079
	0.157 1.09		-45.0 -1.852				0.9169		-0.1164	0.0191
85	0.158 1.14	8 18.19	-45.4 -1.897	5 -1.5095	-0.3765	-0.0194	0.9313	0.0547	-0.1698	0.0151
	0.162 1.20		-45.0 -1.914				0.9638		-0.0767	0.0116
			45 % 0 45 %	2 2400		2 2250	0.00/7	2 2/55	A	2 44.4
	0.144 0.95		-45.0 -2.056				0.8263		-0.1645	0.0116
	0.149 1.00		-45.0 -2.228				0.9072		-0.2590	0.0061
	0.152 1.04		-45.4 -2.235				1.0793		-0.2237 -0.1708	0.0048
	0.157 1.09		-45.0 -2.2620 -45.0 -2.311				1.1129		-0.1700	0.0226
91	Ø.158 1.15	20.24	-45.0 -2.311	2 -1.0/20	-0,300/	-0.0237	1.1154	0.0753	-0,2424	0.0104
92	0.162 1.19	8 20.28	-45.4 -2.3531	-1.2592	-0,3855	-0.0186	1.1597	0.0298	-0.0199	0.0162
	0.147 0.95		-45.0 -2.442				1.0173	0.0964	-0.2316	0.0079
96	0.152 1.00	22.23	-45.0 -2.705				1.1515		-0.2021	0.0070
97	0.155 1.05	22.26	-45.0 -2.702	5 -1.7407	-0.3142	-0.0112	1.3045	0.0923	-0.2727	0.0040
98	0.158 1.09	7 22.27	-45.0 -2.736	-1.9280	-0,3612	-0.0219	1.3509	0.0460	-0.1211	0.0239
0.5									~	
	0.162 1.15		-45.6 -2.789				1.3647		-0.1875	0.0225
	0.165 1.19		-45.6 -2.826				1.4015		-0.0079	0.0198
	0.147 0.95	-	-45.0 -2.942				1,2941	The state of the s	-0.1867	0.0127
	0.152 1.00		-45.0 -3.207				1.4232		-0.2118	0.0057
103	0.155 1.04	24.34	-45.0 -3.200	-1./358	-0,3190	-0.0098	1.6009	0.0910	-0.2184	0.0035
104	0.162 1.09	8 24.34	-45.4 -3.258	-2.0478	-0,3482	-0.0248	1.6377	0.0821	-0.1666	0.0200

TABLE 1.01

#### ROLL ANGLE = -45 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
105	0.162	1.149	24.38	-45.0	-3.5224	-1.8536	-0,3473	-0.0287	1.6617	0.0863	-0.2176	0.0202
106	0,163	1,200	24.44	-45.0	-3.5728	-1.4535	-0,3714	-0.0230	1.7123	0.0416	-0.1620	0.0213
107	0.147	0.951	26.33	-45.0	-3.3765	-1.8345	-0.0811	-0.0123	1.5590	0.1230	-0.2622	0.0113
108	0.154	1.001	26.37	-45.0	-3.6668	-2.0384	-0,1234	-0.0122	1.7284	0.1330	-Ø.2716	0.0034
109	0.157	1.051	26.42	-45.0	-3.7253	-1.9064	-0,3275	-0.0163	1.9356	0.1238	-0.2749	0.0016
110	0.160	1 100	26.42	-45 N	-3.7936	-2.1865	-0.3458	-0.0320	1.9689	0.1039	-0.2356	0.0169
-	0.180	200	26.46		-3.8529				1.9742		-0.3293	0.0138
	0.167		26.52		-3.9095				2.0323		-0,1399	0.0176
100000000000000000000000000000000000000	0.163		28.41		-3.9061				1.8934	-0.0360		0.0195
	0.154		28.46		-4.1659				2.0613		-0.1354	0.0145
114	8.134	1.002	20.40	-45,6	-4.1039	-1.7933	-6,6997	-0.0131	2.0013	D.0255	-6.1354	0.0145
115	0.157	1.048	28.50	-45.0	-4.2179	-1,6345	-0,2962	-0.0178	2,2573	0.0593	-0.1609	0.0131
116	0.162	1.099	28.50	-45.0	-4.5470	-2.2540	-0.3260	-0.0336	2.3313	0.1246	-0.2715	0.0170
117	0.163	1.149	28.55	-45.0	-4.4075	-2.0713	-0.3027	-0.0342	2.3419	0.1316	-0.2973	0.0187
118	0.167	1.200	28.60		-4.4429				2,3954	0.0820	-0.1347	0.0172

TABLE 1.02 DATA LISTINGS

# ROLL ANGLE = -37.5 DEG.

				022 -1102		, n=4.				
SER	REYN MA	H THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
3 4 5	0.139 0.99 0.147 0.99 0.150 1.09 0.154 1.09 0.157 1.14	9 -2.01 50 -2.01 8 -2.01	-37.> 2.1098 -37.> 2.1178 -37.> 2.1036 -37.> 2.1135 -37.> 2.1230	0.1170 0.0152 0.0659	-0.1401 -0.1779 -0.3124 -0.3524 -0.3586	0.0031 0.0144 -0.0073	0.1850 0.3303 0.3488	-0.0028 -0.0001 -0.0072 0.0075 0.0103	0.0461 0.0207	0.0171 0.0170 0.0167 0.0170 0.0165
8 9 10	0.157 1.22 0.142 0.93 0.145 1.00 0.150 1.03 0.154 1.10	51 -0.01 70 -0.01 51 -0.01	-37.5 0.1420 -37.5 -0.0317 -37.5 -0.0386 -37.5 -0.0312 -37.5 -0.0440	-0.0591 -0.0688 -0.0790	-0,1531 -0,1919 -0,3065	0.0061 0.0065 0.0143	0.1592 0.1984 0.3207	-0.0058 -0.0042 -0.0034 -0.0055 0.0073	0.0489 0.0344 0.0374 0.0512 0.0178	0.0169 0.0167 0.0174 0.0153 0.0170
13 14 15	0.157 1.15 0.160 1.15 0.142 0.95 0.147 0.95 0.150 1.06	08 0.01 50 2.01 9 2.01	-37.5 -0.0362 -37.5 -0.0110 -37.5 -0.1621 -37.5 -0.1796 -37.5 -0.1701	0.0042 -0.1967 -0.2403	-0.3631 -0.1554 -0.1911	-0.0090 0.0061	0.3541 0.1670 0.2029	0.0130 -0.0057 -0.0029 -0.0012 -0.0012	-0.0216 0.0448 0.0444 0.0373 0.0626	0.0170 0.0174 0.0178 0.0177 0.0166
18 19 20	0.157 1.09 0.157 1.14 0.160 1.20 0.142 0.94 0.149 1.00	9 2.01 01 2.01 19 4.02	-37.5 -0.1917 -37.5 -0.1869 -37.5 -0.3055 -37.5 -0.3307	-0.2545 -0.1595 -0.3439	-0,3566 -0,3726 -0,1654	-0.0113 -0.0083 0.0042	0.3516 0.3699 0.1906	0.0039 0.0071 -0.0164 -0.0076 -0.0070	0.0136 0.0032 0.0854 0.0564 0.0535	0.0186 0.0191 0.0187 0.0191 0.0197
23 24 25	0.152 1.00 0.157 1.00 0.158 1.15 0.162 1.20 0.142 0.90	9 4.02 50 4.02 11 4.03	-37.5 -0.3100 -37.5 -0.3545 -37.5 -0.3434 -37.5 -0.3261 -37.5 -0.4606	-0.4806 -0.4286 -0.3095	-0,3522 -0,3505 -0,3712	-0.0065 -0.0097 -0.0097	0.3696 0.3639 0.3835	-0.0182 -0.0082 -0.0094 -0.0270 -0.0139	0.0814 0.0570 0.0275 0.1192 0.0718	0.0185 0.0201 0.0206 0.0192 0.0228
3Ø 31 32	0.147 0.99 0.150 1.09 0.154 1.16 0.157 1.19 0.173 1.19	6.04 6.03 6.04	-37.5 -0.4930 -37.5 -0.4914 -37.5 -0.5136 -37.5 -0.5083 -37.5 -0.4825	-0.4982 -0.6388 -0.5940	-0,3078 -0,3574 -0,3488	0.0120 -0.0066 -0.0114	0.3697 0.4028 0.3890	-0.0240 -0.0247 -0.0238 -0.0037 -0.0424	0.1090 0.1103 0.1073 0.0299 0.1812	0.0222 0.0234 0.0232 0.0257 0.0221
35 36 37	0.142 0.90 0.147 0.90 0.150 1.00 0.154 1.10 0.157 1.10	8 8.03 50 8.05 80 8.05	-37.5 -0.6347 -37.5 -0.6737 -37.5 -0.6774 -37.5 -0.6882 -37.5 -0.6873	-0.8370 -0.7105 -0.8035	-0,1858 -0,3182 -0,3602	0.0126 -0.0075	0.2805 0.4223 0.4455	-0.0282 -0.0483 -0.0365 -0.0394 -0.0267	0.1386 0.1963 0.1790 0.1811 0.1198	0.0244 0.0251 0.0271 0.0285 0.0295
40 41 42	0.175 1.26 0.144 0.99 0.149 1.06 0.152 1.09 0.157 1.16	10.05 1 10.05 1 10.07	-37.> -0.6587 -37.> -0.8163 -37.> -0.6590 -37.> -0.8671 -37.> -0.8760	-0.9408 -1.0241 -0.8869	-0.1515 -0.1902 -0.3336	0.0032 -0.0014 0.0080	0.2946 0.3358 0.4878	-0.0503 -0.0552 -0.0685 -0.0552 -0.0515	0.2206 0.2262 0.2788 0.2572 0.2386	0.0271 0.0283 0.0296 0.0299 0.0321
44	0.158 1.14	19 10.07	-37.5 -0.8802	-0.9442	-0.3590	-0.0156	0.4920	-0.0341	0.1625	0.0316

TABLE 1.02 DATA LISTINGS

ROLL ANGLE = -37.5 DEG.

SER	REYN	MACH	THETA	RANG	VORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
45	0.162	1.201	10.08	-37.5	-0.8544	-0.7426	-0.3918	-0.0140	0.5215	-0.0652	0.3302	0.0292
46	0.145	0.948	12.07	-37,5	-1.0155	-1.1428	-0,1574	0.0021	0.3681	-0.0650	0.2827	0.0250
47	0.149	0.999	12.07	-37.5	-1.0747	-1.2422	-0,1964	-0.0004	0.4164	-0.2840	0.3720	0.2277
48	0.152	1.051	12.08	-37.5	-1.0778	-1.0773	-0,3301	0.0095	0.5576	-0.0626	0.2862	0.0270
49	0.155	1.100	12.08	-37.5	-1.0912	-1.1738	-0.3718	-0.0110	0.5811	-0.4783	0.3274	0.0320
50	0.158	1.148	12.10	-37.5	-1.1016	-1.1469	-0,3777	-0.0179	0.5825	-0.0451	0.2386	0.0282
51	0.162	1.199	12.11	-37.5	-1.0690	-0.8914	-0,3936	-0.0164	0.5929	-0.2818	0.3845	0.0271
54	0.142	0.948	14.07	-37.5	-1.2304	-1.3581	-0,1452	0.0025	0.4424	-0.0493	0.2693	0.0128
55	0.147	0.998	14.08	-37.5	-1.3025	-1.4413	-0.1820	-0.0021	0.4913	-0.0843	0.4313	0.0178
	0.150		14.10	-37.5	-1.2891	-1.1574	-0.3210	0.0062	0.6314	-0.0570	0.3123	0.0147
			_		-							
57	0.154	1.101	14.10	-37.5	-1.5186	-1.3620	-0,3691	-0.0135	0.6661	-0.0818	0.3843	0.0239
58	0.157	1.150	14.11	-37.5	-1.3251	-1.2943	-0.3691	-0.0189	0.6626	-0.0660	0.3009	0.0173
	0.160		14.12	-37.5	-1.3017	-1.0049	-0.3968	-0.0160	0.6870	-0.1002	0.4687	0.0158
60	0.142	0.952	16.09	-37.6	-1.4724	-1.6125	-0,1342	0.0003	0.5373	-0.0461	0.2577	-0.0052
	0.147		16.11		-1.5529				0,5939	-0.0676	0.3817	0.0020
_												
62	0,150	1.049	16.13	-37.6	-1.2394	-1.3307	-0.3271	0.0055	0.7470	-0.0398	0.2532	-0.0063
63	0.154	1.130	16.13	-37.5	-1.5789	-1.4966	-0,3802	-0.0155	0.7867	-0.0673	0.3988	0.2088
64	0.157	1.149	16.14	-37.5	-1.5834	-1.4066	-0,3638	-0.0208	0.7697	-0.0723	0.3400	0.0047
65	0.160	1,201	16.17	-37.5	-1.5661	-1.0903	-0,3924	-0.0164	0.7971	-0.0997	0.4859	0.0001
	0.142		18.11	-37.6	-1.7356	-1.8735	-0,1333	-0.0036	0.6627	-0.0421	0.2955	-0.0168
				_								
67	0.145	1.000	18.13	-37.6	-1.8531	-1.9490	-0,1735	-0.0062	0.7356	-0.0431	0.3157	-0.0143
68	0.150	1.048	18.16	-37.6	-1.8135	-1.3665	-0,3249	-0.0010	0.8730	-0.0179	0.1390	-0.0246
69	0.157	1,099	18.16	-37.5	-1.8723	-1.6679	-0,3677	-0.0173	0.9165	-0.0434	0.3204	-0.0002
70	0.157	1,148	18.18		-1.9032				0.9210	-0.0554	0.3280	-0.0090
71	0.160	1,198	18.21	-37.0	-1.9220	-1.2081	-0,3916	-0.0177	0.9560	-0.0945	0.4716	-0.0141
	0.145		47.08		-2.0392					-0.0296		-0.0218
	0.149		20.17		-2.2315				0.9089	-0.0278	0.2661	-0.0202
	0.152		20.22		-2.2156					0.0046		-0.0285
	Ø.155		20.21		-2.2704					-0.0291		-0.0018
76	0.158	1.150	20.24	-37.6	-2.3208	-1.6939	-0,3570	-0.0237	1.1155	-0.0419	0.2395	-0.0086
							12.12.13	TUYEUS T				
	0.162		20.28		-2.3662					-0.0851		-0.0101
	0.142		22.19		-2,4604					-0.0423		-0.0298
	0.147		22.23		-2.7214					-0.0435		-0.0274
	0.150		22.26		-2.7274					-0.0074		-0.0317
83	0.154	1.100	22.26	-37.6	-2.7594	-1.9596	-0,3680	-0.0218	1.3659	-0.0677	0.3032	-0.0018
	0.157		22.30		-2.8175					-0.0764		-0.0061
	0.160		22.34		-2.8428					-0.1046		-0.0077
	0.142		24.25		-2.9571					-0.0316		-0.0428
	0.147		24.30		-3.2027					-0.0638		-0.0349
88	0.150	1,050	24.33	-37.6	-3.2269	-1./484	-0.3107	-0.0159	1.5983	-0.0354	0.1351	-0.0402
0.0		4 100	24 74	-77 .	7 (05.	2 2777	-0 7574			-0 0050	0 7057	- 0 0044
89	Ø.155	1.100	24.34	-3/.0	-3.3071	-2.0/3/	-0,35/6	-0.0208	1.0058	-0.0858	0.305/	-0.0064

TABLE 1.02

#### ROLL ANGLE = -37.5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
90	0.157	1.149	24.38	-37.6	-3.3556	-1.9520	-0,3339	-0.0312	1.6604	-0.0102	0.1992	-0.0138
91	0.160	1.201	24.41	-37.0	-3.3864	-1.5318	-0.3642	-0.0246	1.7092	-0.0360	0.2507	-0.0139
92	0.145	0.950	26.32	-37.6	-3.3993	-1.8458	-0.0730	-0.0176	1.5568	-0.0931	0.3914	-0.0481
93	0.149	0.999	26.37	-37.0	-3.6789	-1.9457	-0.1116	-0.0153	1.7203	-0.1115	0.4464	-0.0378
94	0.152	1.049	26.41	-37.6	-3.7507	-1.8171	-0,3017	-0.0151	1.9249	-0.0617	0.2179	-0.0397
95	0.157	1.100	26.41	-37.0	-3.8389	-2.1887	-0,3459	-0.0319	1.9891	-0.0783	0.2498	-0.0103
96	0,158	1.152	26.46	-37.0	-3.8830	-1.9779	-0,3152	-0.0338	1.9818	-0.0320	0,2268	-0.0127
97	0.162	1.202	26.50	-37.0	-3.9262	-1.6613	-0.3486	-0.0273	2.0394	-0.0233	0.2488	-0.0153
98	0.144	0.952	28.38	-37.6	-3.8924	-1.9863	-0,0563	-0.0178	1.8828	0.1186	0.0896	-0.0541
99	0.149	1.000	28.44	-37.6	-4.1841	-1.9283	-0,0962	-0.0155	2.0637	0.0723	0.1871	-0.0521
100	0.152	1.050	28.48	-37.6	-4.2840	-2.0032	-0,2903	-0.0176	2.2822	0.1140	-0.0244	-0.0484
101	0.170	1.097	28.49	-37.6	-4.3642	-2.3437	-0,3261	-0.0345	2,3378	0.0477	0.1093	-0.0250
102	0.158	1.152	28.53	-37.0	-4.4077	-2.1337	-0,3032	-0.0365	2.3394	0.0323	0.1488	-0.0247
103	0.163	1,201	28.58	-37.6	-4.4684	-1.8372	-0,3428	-0.0293	2.4128	-0.0276	0.2147	-0.0163

TABLE 1.03 DATA LISTINGS

#### ROLL ANGLE = -30 DEG.

						OLL ANDE		0.51				
SER	REYN MA	ACH TI	HETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
3	0.152 0.9	951 -	2.02	-30.0	0.1088	9.9792	-0,1497	0.0088	0.1622	0.0023	0.0247	0.0191
	0.158 1.6			-30.0	0.1148		-0.1828		0.1933	0.0051	0.0189	0.0181
	0.162 1.6			-30.0	0.1040		-0,3127		0.3284	0.0008	0.0415	0.0183
				-			-0,3615		0.3585	0.0081	0.0078	0.0183
	0.163 1.6			-30.0	0.1136				Ø.3479		-0.0264	
'	0.168 1.1	140 -	2.02	-30.0	8.1242	0.1001	-0,3529	-0.0041	0,34/7	0.0133	-6.0204	0.0182
8	0.172 1.2	200 -	2.02	-30.0	0.1486	0.1581	-0,3725	-0.0071	0.3704	-0.0172	0.0461	0.0194
9	0.155 0.9	951 -	0.01	-30.0	-0.0240	-0.0617	-0,1648	0.0080	0.1728	0.0012	0.0275	0.0182
10	0.158 0.9	999 -	0.01	-30.0	-0.0254	-0.0669	-0.1811	0.0062	0.1873	-0.0020	0.0316	0.0177
11	0.162 1.6	752 -1	0.01	-30.0	-0.0292	-0.0861	-0.3137	0.0094	0.3230	-0.0069	0,0439	0.0182
12	0.165 1.6	798 -					-0,3527	-0.0042	0.3484	0.0083		0.0183
	0.168 1.						-0,3475			0.0189	-0.0399	0.0175
	0.172 1.3						-0,3668			-0.0060	0.0423	0.0177
15	Ø.155 Ø.			-30.0	-0.1620	-0.2047	-0,1739	0.0076	0.1870	-0.0036	0.0292	0.0187
16	0.158 1.6	000	2.00	-30.0	-0.1751	-0.2383	-0,1864	0.0042	0.1966	-0.0028	0.0421	0.0186
17	0.162 1.6	050	2.01	-30.0	-0.1690	-0.1930	-0,2955	0.0130	0.3142	-0.0067	0.0527	0.0172
18	0.165 1.	102	2.00	-30.0	-0.1889	-0.2913	-0,3534	-0.0039	0.3558	-0.0052	0.0295	0.0183
19	0.172 1.3	150	2.01	-30.0	-0.1829	-Ø.2636	-0,3554	-0.0078	0.3538	0.0098	-0.0262	0.0197
20	0.173 1.2	200	2.01	-30.0	-0.1669	-0.1754	-0,3633	-0.0067	0.3622	-0.0179	0.2633	0.0180
21	8.152 Ø.S	950	4.01	-30.0	-0.3062	-0.3669	-0,1591	0.0048	0.1848	-0.0117	0.0575	0.0206
22	0.158 1.	000					-0,2004	0.0048	0.2283	-0.0145	0.0847	0.0205
23	Ø.163 1.6	348	4.03	-30.v	-0.3147	-2.3020	-0,2940	0.0120	0.3273	-0.0173	0.0855	0.0200
	0.165 1.						-0.3566			-0.0068	0.0761	0.0211
	0.172 1.						-0,3445			-0.0025	0.0292	0.0221
	Ø.173 1.1						-0,3772			-0.0255	0.1249	0.0208
	0.155 0.9						-0.1607			-0.0277	0.1327	0.0229
	D. 255 D.								0.2147	0.02//	0.1327	
28	Ø.162 1.	001					-0,1921		0.2483	-0.0275	0.1469	0.0232
29	0.165 1.	051	6.03	-30.0	-0.5025	-0.5713	-0.3244	0.0042		-0.0288	0.1471	0.0242
30	0.168 1.	100	6.03	-30.0	-0.5227	-0.6881	-0,3623	-0.0071	0.4081	-0.0277	0.1332	0.0238
31	Ø.172 1.	149	6.03	-30.0	-0.5149	-0.6422	-0,3563	-0.0105	0.3980	-0.0266	0.1053	0.0257
32	0.173 1.2	200	6.04	-30.n	-0,5024	-0.5283	-0,3796	-0.0109	0.4195	-0.0357	0.1671	0.0245
33	0.155 0.	950	8.04	-30.N	-0.6405	-0.8131	-0.1483	0.0047	0.2422	-0.0539	0.2303	0.0264
	0.162 1.						-0,1910			-0.0704	0.2950	0.0263
	Ø.165 1.					-0.7835		0.0079		-0.0547	0.2534	0.0283
	Ø.168 1.						-0,3628			-0.0684	0.2703	0.0289
	Ø.173 1.						-0,3638			-0.0501	0.2023	0.0310
3/	D.1/3 1.	.51	0.05	-30.0	-0.7032	-0.0500	-013030	-0.0113	D. 77/3	-0.0501	0.2020	0.0310
38	Ø.175 1.2	200	8.06	-30.0	-0.6826	-0.6848	-0,3866	-0.0119	0,4666	-0.0675	0.2902	0.0275
41	0.150 0.9	949 1	0.04	-30.0	-0.8419	-1.0480	-0,1452	0.0039	0.2936	-0.0830	0.3575	0.0276
42	0.154 1.6	001 1	0.05	-30.0	-0.8941	-1.1486	-0,1890	0.0013	0.3433	-0.1030	0.4386	0.0291
43	0.157 1.6	148 1	0.06	-30.0	-0.8710	-0.9215	-0,3130	0.0081	0.4683	-0.0799	0.3308	0.0273
	0.160 1.5						-0,364.	-0.0087	0.5071	-0.0969	0.4038	0.0329
45	Ø.163 1.1	151 1	0.06	-30.0	-0.9029	-1.0467	-0,3567	-0.0163	0.4929	-0.0644	0.2927	0.0312

# TABLE 1.03 DATA LISTINGS

### ROLL ANGLE = -30 DEG.

SER	REYN MA	CH THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG SIDE F	YAW M	ROLL M
		40 40 07	-70 4 4 4930		-0 3042	-0.0140	0.5228 -0.0942	0.4403	9 9004
	0.167 1.2		-30.0 -0.8709						0.0294
	0.150 0.9	A TOTAL CONTRACTOR OF THE PARTY	-30.0 -1.0560			0.0014	0.3688 -0.1119	0.4905	0.0206
	0.154 0.9		-30.0 -1.1035			0.0000	0.4220 -0.1425	0.5971	0.0228
	0.157 1.0		-30.0 -1.1122			0.0077	0.5772 -0.1081	0.4885	0.0239
50	0.163 1.1	01 12.08	-30.0 -1.1185	-1.2969	-Ø.3795	-0.0117	0.5936 -0.1273	0.5436	0.0295
51	0.163 1.1	49 12.08	-30.0 -1.1212	-1.2579	-0,3636	-0.0150	0.5754 -0.1059	0.4591	0.0278
52	0.167 1.1	98 12.10	-30.0 -1.0924	-1.0131	-0,3925	-0.0154	0.5976 -0.1351	0.5995	0.0242
53	0.150 0.9	52 14.08	-30.0 -1.2651	-1.5036	-0.1468	-0.0029	0.4471 -0.1322	0.5650	0.0035
54	0.154 1.0	01 14.08	-30.0 -1.3385	-1.5783	-0.1967	-0.0037	0.5127 -0.1731	0.7571	0.0104
	0.157 1.0		-30.0 -1.3090			0.0041	0.6379 -0.1371	0.5951	0.0081
			2.0075		-,		211011 211012		
54	0.163 1.1	00 14.09	-30.0 -1.3533	-1 .4931	-0.3742	-0.0140	0.6789 -0.1631	0.7107	0.0196
	0.167 1.1		-30,0 -1.3602				Ø.6736 -Ø.1432	0.6238	
	Ø.168 1.1		-30.0 -1.3288				0.6877 -0.1798	0.7934	0.0094
	0.150 0.9		-30.1 -1.5111				0.5544 -0.1244	0.5984	
00	0.157 1.0	00 16.10	-30.1 -1.>872	-1.0199	-0,1900	-0.0047	0.6182 -0.1712	0.7542	-0.0000
			77	4 4004					
	0.160 1.0		-30.1 -1.2565				0.7602 -0.1016	0.4932	
	0.163 1.1		-30,0 -1.5941				0.7924 -0.1790	0.8034	
	0.167 1.1		-30,1 -1.6134				0,7726 -0.1672	0.7032	
64	0.168 1.1	99 16.16	-30.1 -1.6003	-1.2476	-0,3878	-0.0163	0.8024 -0.1947	Ø.8535	-0.0067
67	0.147 0.9	51 18.11	-30.1 -1.7556	-1.9645	-0,1366	0,0003	0.6756 -0.1148	0.5664	-0.0394
68	0.152 1.0	00 18.12	-30.1 -1.8756	-2.0475	-0,1741	-0.0087	0.7405 -0.1519	0.7418	-0.0226
69	0.152 1.0	49 18.15	-30.1 -1.8607	-1.6357	-0,3443	0.0003	0.9070 -0.0830	0.4572	-0.0349
70	0.158 1.1	01 18.15	-30.1 -1.8851	-1.8034	-0.3658	-0.0180	0.9177 -0.1695	0.7540	-0.0095
71	0.162 1.1	49 18.17	-30.1 -1.9308				0.9324 -0.1502	0.7034	-0.0188
	0.163 1.1		-30.1 -1.9553				0.9607 -0.1715	0.7816	
				••••					
73	0.144 0.9	51 20.13	-30.1 -2.0743	-2.2027	-0.1252	-0.0096	0.8225 -0.0939	0.5147	-0.0476
	0.152 1.0		-30.1 -2.2433				0.9271 -0.1181		-0.0332
	0.155 1.0		-30.1 -2.2506				1.0927 -0.0868	0.4405	And the second s
	0.158 1.1		-30.1 -2.2816				1.1087 -0.1471		-0.0165
	0.158 1.1		-30.1 -2.5490				1.1313 -0.1429		-0.0289
"	8.130 1.1	47 20.22	-30.1 -2.3490	-1.0/10	-0,3020	-0.021/	1.1313 -0.1429	0.0020	-0.0203
70		00 00 04	-70 4 -7 40-7	4 5422	-0 7747	-0.0107	4 4479 -0 4704	. 7.04	0 0704
	0.165 1.1		-30.1 -2.4013				1.1678 -0.1386		-0.0321
	0.147 0.9		-30.1 -2.4940				1.0260 -0.0971		-0.0535
	0.149 0.9		-30.1 -2.7093				1.1510 -0.1481		-0.0411
	0.155 1.0		-30.1 -2.7230				1.3339 -0.0753	0.4013	
82	0.158 1.0	99 22.25	-30.1 -2.7656	-2.1329	-0,3561	-0.0218	1.3569 -0.1635	0.6787	-0.0198
	0.162 1.1		-30.1 -2.8361				1.3653 -0.1453	0.6210	-0.0326
84	0.163 1.2		-30.1 -2.8930	-1.6077	-0.3731	-0.0205	1.4256 -0.1312	0.6020	-0.0341
85	0.147 0.9	51 24.24	-30.1 -2.9765	-2.3216	-0,0995	-0.0145	1.2996 -0.1480	0.6743	-0.0660
	0.152 0.9		-30.1 -3.2212				1.4422 -0.1940	0.8439	Carl C. Land St. Co. Co. Common
	0.155 1.0		-30,1 -3,2688				1.6371 -0.1232		-0.0638
					-,				
88	0.158 1.0	99 24.34	-30.1 -3.3007	-2.241B	-0.3505	-0.0223	1.6591 -0.1652	0.7244	-0.0320
-0					2,000	2.2220			

TABLE 1.03

### ROLL ANGLE = -30 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M ROLL M
89	0.163	1.151	24.36	-30.1	-3.3589	-2.1736	-0,3421	-0.0234	1.6757	-0.0980	0.5341 -0.0422
90	0.167	1.200	24.41	-30.1	-3.4159	-1.7438	-0,3669	-0.0226	1.7252	-0.0939	0.5220 -0.0417
91	0.150	0.951	26.31	-30.1	-3.4759	-2.1611	-0,0826	-0.0190	1.5980	-0.2171	0.8681 -0.0847
92	0.154	1.002	26.37	-30.1	-3.7137	-2.0362	-0,1203	-0.0149	1.7441	-0.2399	1.0115 -0.0725
93	0.155	1.048	26.40	-30.1	-3.7797	-2.0259	-0,2938	-0.0152	1.9301	-0.1402	0.6148 -0.0747
94	0.160	1.100	26.41	-30.1	-3.8594	-2,3617	-0,3323	-0.0270	1.9900	-0.1331	0.6245 -0.0443
95	0.162	1.148	26.44	-30.1	-3.9205	-2.2793	-0,3272	-0.0333	2.0089	-0.0611	0.4933 -0.0486
96	0.167	1.198	26.50	-30.1	-3.9548	-1.8383	-0,3442	-0.0278	2.0475	-0.1081	0.5623 -0.0427
97	0.147	0.948	28.38	-30.1	-3.9648	-2.1139	-0,0466	-0.0217	1.9065	-0.1631	0.7297 -0.0895
98	0.154	1.002	28.45	-30.1	-4.2254	-1.9879	-0,0927	-0.0174	2.0789	-0.1767	0.9461 -0.0749
99	0.157	1.049	28.48	-30.1	-4.5327	-2.1136	-0,2816	-0.0176	2.2979	-0.0786	0.5598 -0.0791
100	8.168	1.100	28.48	-30.1	-4.4848	-2.4676	-0.3159	-0.0313	2.3507	-0.0855	0.6181 -0.0570
101	0.163	1.150	28.53	-30.1	-4.4565	-2.3333	-0,2937	-0.0344	2.3560	-0.1173	0.6049 -0.0558
102	0.167	1.200	28.57	-30.1	-4.5034	-2.0173	-0,3246	-0.0295	2.4131	-0.1138	0.6001 -0.0535

TABLE 1.04 DATA LISTINGS

ROLL ANGLE = -22.5 DEG.

SER	REYN M	ACH '	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
2	Ø.152 Ø.	954	-2.01	-22.5	0.1114	9 9497	-0,1588	0.0094	0.1720	0 4020	-0.0160	0.8171
	0.157 1.			-22.5	0.1228		-0,1947	0.0057		-0.0016	0.0477	0.0172
			-2.01		8.1076		-0.3032	0.0122		-0.0014		0.0158
	0.160 1.		-2.02	-22.5								
	0.163 1.		-2.01	-22.5	0.1146		-0,3597		0.3569		-0.0166	0.0171
•	0.168 1.	151 .	-2.01	-22.5	3,1235	0,0905	-0,3467	-0.0107	0,3399	0.0100	-0.0313	0.0164
7	0.168 1.	198 -	-2.01	-22.5	2.1467	0.1698	-0,3638	-0.0083	0.3604	-0.0071	0.0657	0.0169
8	0.152 0.	951 .	-0.01	-22.5	-0.0275	-0.0689	-0,1578	0.0081	0.1659	-0.0016	0.0290	0.0155
9	0.158 1.	003 .	-0.01	-22.5	-0.0323	-0.0759	-0,2003	0.0073	0.2075	0.0092	0.0125	0.0170
10	0.163 1.	049 .	-0.01		-0.0351			0.0146	0.3261	-0.0045	0.0346	0.0163
11	0.165 1.	102	-0.01	-22.5	-0.0425	-0.1195	-0,3571	-0.0058	0.3513	0.0132	0.0028	0.0169
12	Ø.168 1.	148 -	-0.01	-22.5	-0.0292	-0.0752	-0.3508	-0.0102	0.3405	0.0012	-0.0194	0.0164
13	0.172 1.	198	-0.01	-22.5	-0.0084	0.0034	-0.3588	-0.0082	0.3505	-0.0154	0.0928	0.0165
	0.155 0.		2.00	-22.5	-0.1628	-0.2098	-0.1601	0.0063	0.1719	-0.0040	0.0339	0.0177
	Ø.158 Ø.		2.01	-22.5	-0.1768	-0.2576	-0.1911	0.0066	0.2038	-0.0031	0.2436	0.0173
-	0.162 1.	-	2.01	-22.5	-0.1774	-0.2376	-0,3366	0.0141	0.3566	-0.0060	0.0635	0.0167
	0.165 1.		2.01				-0.3506		0.3535	0.0072	0.0135	0.0173
	0.168 1.		2.00				-0,3485		0.3460		-0.0173	0.0186
	0.173 1.		2.01				-0,3704			-0.0160	0.0928	0.0177
	0.155 0.		4.02	-22.5	-0.3142	-0.3918	-0,1613	0.0080		-0.0124	0.0701	0.0192
21	0.158 1.	001	4.01	-22.5	-0.5417	-0,4758	-0,1918	0.0042	0.2194	-0.0098	0.0659	0.0192
22	0.162 1.	050	4.02	-22.5	-0.3370	-0.4088	-0,3282	0.0130	0.3640	-0.0210	0.0881	0.0207
	0.165 1.		4.02				-0,3501	-0.0060	0.3686	-0.0101	0.0701	0.0206
24	0.172 1.	149	4.02	-22.5	-0.3535	-0.4732	-0.3509	-0.0109	0.3640	-0.0053	0.0035	0.0217
25	0.173 1.	200	4.02	-22.5	-0.3340	-0.3669	-0.3786	-0.0096	0.3914	-0.0282	0.1335	0.0204
28	Ø.168 Ø.	950	6.02	-22.5	-0.4814	-0.6417	-0,1579	0.0047	0.2122	-0.0347	0.1510	0.0232
_	0.154 0.		6.02				-0,1825			-0.0333	0.1799	0.0221
	0.160 1.		6.02		-0.5236			0.0110		-0.0279	0.1439	0.0239
	0.163 1.		6.02				-0,3531			-0.0307	0.1617	0.0225
	0.183 1.		6.02				-0,3460			-0.0218	0.0883	0.0251
33	0.168 1.	199	6.04	-22.5	-0.5077	-0.5715	-0,3711	-0.0121	0.4103	-0.0437	0.2111	0.0223
34	Ø.165 Ø.	950	8.03	-22.5	-0.6766	-0.9421	-0.1563	0.0043	0.2535	-0.0596	0.2464	0.0242
	Ø.157 Ø.		8.03				-0,1973	0.0006	0.2963	-0.0736	0.2992	0.0232
36	0.160 1.	049	8.04		-0.7194			0.0064	0.4335	-0.0590	0.2609	0.0257
11.00	0.163 1.		8.04				-0,3874	-0.0101		-0.0629	0.3070	0.0269
	0.168 1.		8.04				-0,3629			-0.0454	0.2069	0.0273
	0.168 1.		8.05				-0,3981			-0.0788	0.3350	0.0250
40	0.152 0.	951 :	10.04		-0.8795			0.0003	0.3160	-0.0992	0.4238	0.0226
	Ø.172 Ø.		10.04				-0,2041			-0.1102	0.4713	0.0250
	0.162 1.		10.05		-0.9258			0.0085		-0.0805	0.3861	0.0245
43	0.165 1.	100	10.05	-22.5	-0.9410	-1.2639	-0,3829	-0.0121	0,5293	-0.1047	0.4720	0.0275
44	Ø.168 1.	150	10.06	-22.5	-0.9333	-1.2073	-0,3662	-0.0174	0,5064	-0.0892	0.3719	0.0301

TABLE 1.04 DATA LISTINGS

### ROLL ANGLE = -22,5 DEG.

SER	REYN MACH	H THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
45	Ø.172 1.199	10.07	-22.5 -0.9173	-0 9855	-0.4055	-0.0150	0.5427	-0.1096	0.4998	0.0268
	Ø.155 Ø.951		-22.5 -1.0898					-0.1533	0.6370	0.0148
			-22.5 -1.1460					-0.1727	0.7257	0.0179
	0.158 0.999									
	0.162 1.049		-22.5 -1.1341					-0.1258	0.5183	0.0170
49	0.165 1.099	12.07	-22.5 -1.1609	-1.4936	-0,3877	-0.0129	0,6092	-0.1588	Ø.6987	0.0252
50	0.172 1.149	12.08	-22.5 -1.1623	-1.4270	-0.3746	-0.0187	0.5908	-0.1317	0.6009	0.0232
	0.173 1.201		-22.5 -1.1345					-0.1557	0.6924	0.0216
	0.155 0.951		-22.0 -1.3221					-0.1681	0.7295	-0.0053
	0.175 0.999		-22.5 -1.3978					-0.2063	0.9032	0.0029
	0.165 1.056		-22.5 -1.3788					-0.1732	0.7382	0.0005
		-								
	0.165 1.100		-22.5 -1.4082					-0.2058	0.9228	0.0107
	0.172 1.149		-22.5 -1.4031					-0.1830	0.7925	0.0070
57	0.173 1.198		-22.5 -1.3746					-0.2134	0.9064	0.0068
	0.155 0.951		-22.6 -1.5446	-1.9342	-0,1479	-0.0072	0.5632	-0.1527	0.7398	-0.0318
59	0.162 1.000	16.10	-22.6 -1.6534	-2.0802	-0.1918	-0.0101	0.6331	-0.2151	0.9847	-0.0120
60	0.165 1.051	16.12	-22.6 -1.6397	-1.7977	-0.3540	-0.0007	0.7947	-0.1922	0.8508	-0.0184
	0.168 1.101		-22.0 -1.6518					-0.2435		-0.0033
	0.173 1.156		-22.6 -1.6659					-0.2019		-0.0073
								-0.2019		-0.0089
	0.176 1.199									
00	0.147 0.951	18.09	-22.6 -1.8006	-2.2250	-6,12//	-0.0045	0.0720	-0.1292	0.0/31	-0.0502
67	0.152 0.999	18.11	-22.6 -1.9522	-2.3831	-0,1699	-0.0114	0.7575	-0.1894	0.8814	-0.0272
68	0.157 1.052	18.14	-22.6 -1.9334	-2,0176	-0.3648	-0.0046	0.9442	-0.1695	0.7974	-0.0314
	0.175 1.101		-22.6 -1.9501	-2.0823	-0.3674	-0.0190		-0.2158		-0.0148
70	0.163 1.152	18.16	-22.6 -1.9907	-1.9888	-0.3603	-0.0229	-	-0.1874		-0.0204
	0.180 1.198		-22.0 -2.0227					-0.2009		-0.0212
1000	0.150 0.950		-22.6 -2.1349					-0.1376		-0.0557
_	0.154 1.000		-22.6 -2.3016					-0.1817		-0.0373
	0.172 1.056		-22.6 -2.3067				1.1169	-0.1361		-0.0423
75	0.162 1.098	20.18	-22.6 -2.3406	-2.3190	-Ø.3637	-0.0201	1.1302	-Ø.1848	0.8800	-0.0235
76	0.163 1.149	20.21	-22.0 -2.4137	-2.1777	-0.3592	-0.0234	1.1492	-0.1575	0.8007	-0.0314
77	0.167 1.208	20.26	-22.6 -2.4710	-1 8170	-0.3770	-0.0100	1 1015	-0.1996	0 0070	-0.0333
	0.150 0.952		-22.6 -2.5544					-0.1208		-0.0630
	0.154 1.002		-22.6 -2.7573					-0.1635		-0.0494
									100000000000000000000000000000000000000	
	0.157 1.050		-22.6 -2.7606					-0.1197		-0.0537
81	0.160 1.100	22.25	-22.6 -2.7923	-2.43/6	-0,3636	-0.0214	1.3740	-0.1626	0.82/4	-0.0302
	0.163 1.148		-22.6 -2.8907	-2.3645	-0,3477	-0.0252	1.3943	-0.1311	0.7221	-0.0436
83	0.167 1.198	22.33	-22.6 -2.9485				1.4491	-0.1789	0.8631	-0.0441
84	0.150 0,950	24.22	-22.0 -3.0460	-2.9280	-0.0864	-0.0149	1.3147	-0.0665	0.5320	-0.0788
	0.154 1.000		-22.0 -3.2650					-0.1714	0.9154	-0.0682
86	0.158 1.047	24.31	-22.0 -3.2633	-2.2728	-0,3067	-0.0156	1.6089	-0.1252	0.6737	-0.0764
87	0.163 1.102	24.32	-22.6 -3.3258	-2.6345	-0,3508	-0.0248	1.6666	-0.0984	0.7180	-0.0424

TABLE 1.04

# ROLL ANGLE = -22,5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
88	0.167	1.149	24.36	-22.6	-3.4082	-2.4724	-0.3451	-0.0264	1.6957	-0.1218	0.7244	-0.0527
89	0.168	1,198	24.40	-22.0	-3.4833	-2.1180	-0,3697	-0.0224	1.7554	-0.1148	0.6920	-0.0582
90	0.150	0.950	26.29	-22.6	-3.5512	-2.7682	-0.0608	-0.0172	1.6122	-0.1673	0.7778	-0.0989
91	0.157	1.000	26.35	-22.6	-3.7863	-2.5978	-0.1119	-0.0189	1.7642	-0.1939	1.0331	-0.0801
92	0.160	1.050	26.39	-22.0	-3.8375	-2.4798	-0.3081	-0.0210	1,9627	-0.1702	0.8691	-0.0903
93	0.163	1.098	26.40	-22.0	-3.9269	-2.7904	-0,3296	-0.0273	2.0168	-0.1386	0.8147	-0.0634
94	Ø.167	1.149	26.43	-22.6	-3.9763	-2.6640	-0,3113	-0.0288	2.0230	-0.0759	0.6566	-0.0671
95	0.168	1,199	26.48	-22.0	-4.0286	-2,2456	-0.3458	-0.0241	2.0847	-0.1112	0.7115	-0.0677
96	0.152	0.950	28.36	-22.0	-4.0846	-2.8589	-0.0321	-0.0178	1.9530	-0.0547	0,5956	-0.1054
97	0.172	1.001	28.43	-22.6	-4.3020	-2.5532	-0.0793	-0.0181	2.1021	-0.1106	0.8910	-0.0919
98	0.162	1.051	28.46	-22.6	-4.4043	-2.6852	-0.2901	-0.0199	2.3365	-0.2486	0.6272	-0.1027
99	0.165	1.100	28.47	-22.6	-4.4797	-2.9392	-0.3053	-0.0309	2.3772	-0.0952	0.7771	-0.0775
100	0.168	1.152	28.52	-22.6	-4.5337	-2.7100	-Ø.2954	-0.0319	2.3949	-0.1343	0.8424	-0.0762
102	0.172	1.199	28.57			-2.4281				-0.1086		-0.0761

TABLE 1.05 DATA LISTINGS

# ROLL ANGLE = -15 DEG.

SER	REYN MAC	H THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
2	0.155 0.95	1 -2.02	-15.0 3.1096	0.0846	-0.1548	0.0091	Ø.1676	0.0096	-0.0105	0.0180
	0.158 1.00		-15.0 0.1210		-0.1851		0.1944		-0.2005	0.0184
					-0.3060	0.0129		-0.0115		
	0.163 1.04		-15.0 0.1112							0.0171
	0.165 1.09		-15.0 0.1143		-0,3559		0.3545		-0.0336	0.0177
6	0.168 1.14	9 -2.02	-15.0 0.1266	0.1045	-0.3480	-0.0087	0.3435	0.0093	-0.0566	0.0179
	0.172 1.19		-15.0 0.1458					-0.0044	0.0220	0.0187
8	0.155 0.95	2 -0.01	-15.0 -0.0242	-0.0548	-0,1627	0.0076	0.1703	0.0074	0.0142	0.0173
9	0.158 1.00	2 -0.01	-15.0 -0.0272	-0.0655	-0,2046	0.0059	0.2104	0.0051	0.0066	0.0176
10	0.163 1.04	9 -0.01	-15.0 -0.0314	-0.0845	-0.3037	0.0109	0.3145	0.0089	0.0172	0.0168
11	0.165 1.09	9 -0.01	-15.0 -0.0341	-0.0974	-0,3525	-0.0042	0.3483	0.0103	0.0073	0.0177
12	0.172 1.15	0 -0.01	-15.0 -0.0288	-0.0788	-0.3525	-0.0078	0.3447	0.0190	-0.0518	0.0172
	0.173 1.20		-15.0 -0.0075					-0.0140	0.0809	0.0185
	Ø.155 Ø.95		-15.0 -0.1650			0.0062	0.1708	0.0012	0.2133	0.0186
	0.162 1.00		-15.0 -0.1816			0.0058	0.2119	0.0023	0.0263	0.0185
	0.165 1.05		-15.0 -0.1876			0.0132		-0.0071	0.0399	0.0183
10	D.165 1.05	2.01	-17.0 -0.1000	0.2410	-0,01//	W.0132	0.00/2	-0.00/1	0,0077	0.0103
17	0.168 1.09	9 2.00	-15.0 -0.1933	-0.3010	-0,3601	-0.0033	0.3633	0.3048	0.0076	0.0185
	0.172 1.14		-15.0 -0.1859	-0.2722	-0.3432	-0.0091	0.3403	0.0146	-0.0549	0.0192
-	0.173 1.19		-15.0 -0.1619					-0.0198	0.2762	0.0177
	0.172 0.94		-15.0 -0.3182			0.0054		-0.0057	0.0496	0.0209
	0.162 1.00		-15.r -2.3520					-0.0136	0.0633	0.0204
	D1102 11-0	- 4.01	171.		2,2200	D. 2202		0.0130	,,,,,,,	0.020
22	0.183 1.04	9 4.02	-15.6 -0.3379	-0.3643	-0,3058	0.0076	0.3358	-0.0136	0.0524	0.0210
-	0.188 1.10		-15.0 -0.3634	-0.5068	-0.3563	-0.0047	0.3759	-0.0083	0.0388	0.0221
	0.173 1.14		-15.0 -0.3575					-0.0029	0.0036	0.0229
	0.195 1.20		-15.0 -0.3414					-0.0224	0.3957	0.0217
	0.158 0.94		-15.0 -0.4984					-0.0219	0.1126	0.0245
										-
	0.162 0.99		-15,0 -0.5386	-0.8128	-0,1937	0.0028	0.2519	-0.0417	0.1544	0.0248
28	0.165 1.04	8 6.03	-15.0 -0.254	-0.6655	-0.3181	0.0069	0.3784	-0.4266	0.1253	0.0256
29	0.168 1.09	9 6.03	-15.0 -0.0542				0.4176	-0.0355	0.1448	0.0246
30	Ø.173 1.15	1 6.03	-15.0 -0.5430	-0.7667	-0.3426	-0.0128	0.3849	-0.0144	0.0425	0.0265
31	0.175 1.19	9 6.04	-15.0 -0.5243	-0.6306	-0,3917	-0.0137	0.4309	-0.0454	0.1743	0.0252
32	Ø.158 Ø.94	8 8.03	-15.0 -0.7057	-1 0530	-0.1584	0.0013	0.2560	-0.0526	0.1970	0.0268
	0.162 1.00		-15.0 -0.7525			0.0025		-0.0640	0.2645	0.0259
	0.167 1.05		-15.0 -0.7402			0.0045		-0.0507	0.1914	0.0273
1717										
_	0.188 1.09		-15.0 -0.7656					-0.0592	0.2442	0.0268
36	0.190 1.15	1 8.04	-15.0 -0.7525	-1.0790	-0,3640	-0.0152	0,4506	-0.0452	0.1405	0.0301
	0.195 1.19		-15.0 -0.7320			-0.0165	0.4811	-0.0619	0.2655	0.0276
41	0.147 0.95	2 10.03	-15.0 -0.9215	~1.3818	-0,1474	0.0010	0,3067	-0.0726	0.3107	0.0234
42	0.152 1.00	1 10.04	-15.0 -0.9738	-1.4861	-0,1943	-0.0014	0.3596	-0.1022	0.3969	0.0269
43	0.155 1.04	9 10.05	-15.0 -0.9718	-1.3544	-0,3399	0.0075	0.5115	-0.0807	0.3195	0.0270
44	Ø.175 1.18	2 10.04	-15.0 -0.7802				0.5260	-0.0978	0.4054	0.0281
45	0.163 1.15	2 10.05	-15.0 -0.9754	-1.3584	-0,3665	-0.0183	0,5130	-0.0624	0.2846	0.0301

# TABLE 1.05

# ROLL ANGLE = -15 DEG.

				OLL AND		OL I				
SER	REYN MACH	THETA	RANG HORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
44	0.180 1.198	10.06	-15.0 -0.9485	-1 1797	-0.3030	-0.0154	0 5384	-0.0996	0.4220	0.0281
	Ø.150 Ø.952	12.04	-15.0 -1.1511					-0.1345	0.5533	0.0140
	0.152 0.999	12.05	-15.4 -1.2079					-0.1269	0.5310	0.0188
	0.157 1.049		-15.0 -1.1948			0.0009		-0.1233	0.4512	0.0158
	0.160 1.101	12.06	-15.0 -1.2172	-1.5/04	-0.3470			-Ø.1496	0.4312	0.0225
96	0.100 1.101	12.00	-15.6 -1.21/2	-1.0993	-0,3020	-6.0192	0.0130	-0.1490	0.0135	0.2223
51	0.163 1.149	12.07	-15.0 -1.2038				0.5995	-0.1204	0.4979	0.0245
52	0.167 1.200	12.08	-15.0 -1.1784	-1.3739	-0.3989	-0.0166	0.6204	-0.1387	0.6046	0.0244
53	0.163 0.951	14.06	-15.0 -1.3910	-2.0233	-Ø.1495	-0.0069		-0.1701		-0.0009
54	0.154 1.000	14.07	-15.0 -1.4617	-2.0847	-0.1973	-0.0072		-0.1730	0.7413	0.0056
55	0.157 1.052	14.08	-15.0 -1.4427	-1.8399	-0,3665	-0.0077	0.6990	-0.1508	0.6407	0.0021
56	0.178 1.101	14.08	-15.0 -1.4737					-0.1877	0.7789	0.0120
57	0.180 1.150	14.09	-15.0 -1.4645	-1.8962	-0,3708	-0.0186	0,6982	-0.1636	0.6827	0.0117
58	0.183 1.202	14.11	-15.6 -1.4430				0.7273	-0.1730	0.7724	0.0103
59	0.163 0.948	16.08	-15.1 -1.6198	-2.2541	-0.1445	-0.0090	0,5788	-0.1605	0.6649	-0.0275
60	0.154 1.001	16.08	-15.1 -1./367	-2.4037	-0,1893	-0.0074	0.6560	-0.1896	0.8070	-0.0065
61	0.157 1.051	16.10	-12.1 -1.7217	-2 1169	-0.3657	-0.0058	Ø 8235	-0.1708	0 7407	-0.0092
	0.162 1.097	16.10	-15.0 -1.7320					-0.2134		0.0026
	0.167 1.150	16.12	-15.0 -1.7420					-0.1710		-0.0005
	0.168 1.200	16.14	-15.1 -1./256	-1 7002	-0.4111	-0.0107		-0.2146		-0.0010
	0.150 0.948	18.08	-15.1 -1.8966				The second second second	-0.1190		-0.0374
									_	
-	0.154 1.000	18.10	-15.1 -2.0352					-0.1656	0.7734	-0.0138
	0.157 1.050	18.13	-15.1 -2.0380				0.9632	-0.1559	0.7615	-0.0168
	0.160 1.101	18.14	-15.1 -2.0380					-0.1891		-0.0018
	0.163 1.150	18.15	-15.1 -2.0697					-0.1783		-0.0100
72	0.167 1.202	18.18	-15.1 -2.0926	-1.9799	-0,4004	-0.0200	1.0145	-0.1991	0.8733	-0.0122
73	0.150 0.950	20.11	-15.1 -2.2378	-2.9119	-0.1216	-0.0101	0.8743	-0.2984	0.5147	-0.0406
	0.154 1.000	20.14	-15.1 -2.4142					-0.1437		-0.0244
	0.157 1.052	20.17	-15.1 -2.4341					-0.1475		-0.0231
	0.160 1.102	20.18	-15.1 -2.4250					-0.1823		-0.0079
	0.163 1.151	20.21	-15.1 -2.4936					-0.1532		-0.0173
							4 2005	0 4530	0.0044	0.0057
	0.167 1.199	20.24	~15.1 -2.5417					-0.1572		-0.0257
	0.150 0.951	22.15	-15.1 -2.6728					-0.0913		-0.0468
	0.154 1.002	22.19	-15.1 -2.8762					-0.1622		-0.0363
	0.160 1.052	22.23	-15.1 -2.9127					-0.1521		-0.0366
82	0.163 1.101	22.24	-15.1 -2.9109	-2,8533	-0,3520	-0.0197	1.4093	-0.1381	0.7857	-0.0160
83	0.167 1.150	22.27	-15.1 -2.9786	-2.7088	-0,3492	-0.0241	1.4296	-0.1418	0.7123	-0.0262
84	0.168 1.198	22.31	-15.1 -3.0306	-2.2990	-0,3793	-0.0208		-0.1676	0.8132	-0.0295
85	0.150 0.951	24.21	-15.1 -3.2160	-3.4348	-0,0858	-0.0144	1.3841	-0.0423	0.4257	-0.0629
86	0.157 0.999	24.27	-15.1 -3.4214				1.5117	-0.1892	0,9194	-0.0527
87	0.160 1.051	24.30	-15.1 -3.4633	-3.0100	-0,3274	-0.0073	1.7157	-0.1878	0.8947	-0.0571
88	0.163 1.100	24.31	-15.1 -3.4575	-3.0635	-0,3417	-0.0234	1.7134	-0.1367	0.7886	-0.0288

TABLE 1.05

#### ROLL ANGLE = -15 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
90	Ø.167	1.148	24.34	-15.1	-3.5224	-2.9099	-0.3364	-0.0271	1.7336	-0.0827	0.6313	-0.0360
91	0.168	1.199	24.40	-15.1	-3.7761	-2.4786	-0,3703	-0.0220	1.7943	-Ø.0953	0.6782	-0.0423
92	0.152	0.952	26.28	-15.1	-3.7193	-3.3463	-0,0626	-0.0215	1.6840	-0.1731	0.7874	-0.0763
93	0.157	1.002	26.35	-15.1	-5.9041	-3,0035	-0,1124	-0.0161	1.8191	-0.2571	1.1432	-0.0641
94	0.160	1.048	26.38	-15.1	-3.9487	-2.8535	-0.2859	-0.0131	1.9990	-0.2256	1.0508	-0.0773
95	0.163	1.098	26.39	-15.1	-4.0284	-3,2232	-p,3326	-0.0245	2.0628	-0.1957	0.9878	-0.0497
96	0.167	1.148	26.42	-15.1	-4.0706	-3.0227	-0.3152	-0.0277	2.0689	-0.1270	0.8113	-0.0522
97	0.168	1.198	26.47	-15,1	-4.1252	-2.6654	-0,3410	-0.0224	2.1243	-0.1291	0.7763	-0.0555
98	0.152	0.948	28.35	-15.1	-4.2400	-3.4215	-0,0333	-0.0125	2.0317	-0.0535	0.5435	-0.0764
99	0.157	1.003	28.43	-15.1	-4.4396	-2.9618	-0,0919	-0.0130	2.1829	-0.1106	0.8588	-0.0703
100	0.162	1.052	28.45	-15.1	-4.5662	-3.2900	-0,2939	-0.0161	2.4194	-0.0945	0.7513	-0.0761
101	0.163	1.100	28.46	-15.1	-4.5790	-3.3726	-0,3006	-0.0260	2.4239	-0.0919	0.7908	-0.0615
102	0.168	1,152	28.51	-15.1	-4.6140	-3.1312	-0,2905	-0.0269	2.4338	-0.1680	0.8800	-0.0618
103	0.172	1,199	28.55	-15.1	-4,6776	-2.8358	-0,3214	-0.0241	2.4972	-0.1560	0.8173	-0.0650

TABLE 1.06

### ROLL ANGLE = -7.5 DEG.

SER	REVN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
JER	WE 1.4	TACH	INC IA	MANO	TOMPAL	rich	AAIAL	BASE	DRAG	SIUL F	1 4 4 11	HOLL II
126	0.145	0.949	-2.02	-7.5	0.1096	0.0715	-0.1599	0.0073	0.1709	-0.0048	-0.2063	0.0180
		0.998	-2.02	-7.5	3.1182		-0.1779	0.0065	0.1884	0.0013		0.0176
		1.050	-2.02	-7.5	1.1076	0.0247	-0.3048	0.0088	0.3171	-0.0036	0.2350	0.0182
		1.101	-2.02	-7.5	3.1150	0.0584	-0.3487	-0.0085	0.3440	0.0114	-0.0045	0.0183
130	0.158	1.150	-2.02	-7,5	0.1248	0.0846	-0.3480	-0.0108	0.3412	0.1236	-0.0766	0.0182
		1.199	-2.02		0.1486					-0.2035		0.0180
		0.949	-0.01		-0.0239			0.0072	0.1621		-0.0050	0.0170
		0.998	-0.01		-0.0278			0.0061	0.1870	0.0054	0.0128	0.0178
-		1,048	-0.01		-0.0296			0.0139		-0.0050	0.0685	0.0163
135	0.150	1,193	-0.01	-/.5	-0.0324	-0.1054	-0,35//	-0.0059	0.3518	0.0035	-0.0006	0.0180
136	0.162	1.150	-0.01	-7.5	-0.0298	-0 0868	-0.3403	-0.0104	0.3389	0 0000	-0.0708	0.0184
		1.201	0.01		-0.0104					-0.0151	0.0814	0.0161
_		0.952	2.01		-0.1626			0.0064	0.1635	0.0015	0.0050	0.0186
-		0.999	2.00		-0.1802			0.0057		-0.0071	0.0159	0.0184
		1.049	2.01		-0.1806			0.0131		0.0018	0.2480	0.0182
										-		
141	0.162	1.098	2.01	-7.5	-0.1936	-0.3079	-0,3613	-0.0062	0.3616	0.3037	0.0143	0.0189
142	0.163	1.151	2.01		-0.1847				0.3416	0.0053	-0.0512	0.0191
		1.201	2.01		-0,1687					-0.0203	0.0976	0.0187
_		0.949	4.02		-0.3210	The second second		0.0035		-0.0002	0.0200	0.0213
145	0.152	0.998	4.02	-7.5	-0.3531	-0.5287	-0,1949	0.0030	0.2221	-0.0006	0.0308	0.0213
114	a 157	1.052	4.02	-7 5	-0.5524	-0 4456	-0 3004	0.0126	0 7450	-0 0075	0.0385	2 224 8
		1.100	4.02		-0.3686	the state of the same of the s				-0.0075 0.0014	0.0329	0.0218
_	-	1.148	4.02		-0.3610			73		0.0061		0.0230
_		1.202	4.02		-3.3458					-0.0117	0.0584	0.0210
		0.950	6.01		-0.2159					-0.0118	0.0535	0.0248
					-							
151	0.157	1.001	6.01	-7.5	-0.5542	-0.8692	-0,1996	0.0009	0.2576	-0.0055	0.2618	0.0251
		1.049	6.02	-7.5	-0.5347	-0.7035	-0.3200	0.0075		-0.2064	0.0841	0.0249
		1.099	6.02		-0.0675				0.4181	-0.0114	0.0637	0.0251
		1.149	6.02		-0.5556					0.0007		0.0265
155	0.168	1.199	6.03	-7.5	-3.>313	-0.6618	-0,3891	-0.0150	0.4278	-0.0353	0.1434	0.0238
		0.950	8.02	-7 -	- 1 2047	4 4047	-0 4504	0 0004	7 2502		2 1012	0.0000
		1.002	8.02		-0.7267 -0.7736			0.0006		-0.0161 -0.0259	0.1210	0.0262
		1.048	8.03		-0.7613			0.0084		-0.0259	0.1090	0.0266
		1.099	8.03		-0.7837					-0.0197	0.1309	0.0270
200		1.152	8.04		-0.7684					-0.3117	0.0247	0.0282
			0,			1.170	2,0002	,	2,,,,,	2,011,	5,02,7	
161	0.168	1.198	8.05	-7.5	-0.7416	-0.9479	-0,3983	-0.0169	0.4815	-0.0437	0.2041	0.0262
164	0.145	0.948	10.03	-7.5	-0.9394	-1.4774	-0,1538	0.0014	0.3165	-0.0335	0.1772	0.0218
_		0.998	10.03		-1.0007			-0.0035	0.3789	-0.0473	0.2131	0.0259
		1.049	10.04		-0.9925			0.0056		-0.0322	0.1575	0.0244
167	0.155	1.102	10.04	-7.5	-1.0057	-1.5288	-0,3900	-0.0157	0.5438	-0.0469	0.2290	0.0271
140		4 150		7 .	1 (100			2 22.1	0. 5040	0.0464	0 .075	a ann:
108	0,158	1.150	10.05	-/.5	-3.9971	-1.4648	-0,3778	-0.0214	0.5248	-0.0184	0.1072	0.0286

TABLE 1.06
DATA LISTINGS

### ROLL ANGLE = -7,5 DEG.

SER REYN MACH	THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
169 0.162 1.201	10.06	-7.5 -4.9782	-1.2460	-0.4136	-0.0204	0.5566	-0.3448	0.2320	0.0271
170 0.157 0.950	12.04	-7.5 -1.1867					-0.0594	0.2769	0.0160
171 0.149 1.002	12.05	-7.5 -1.2490				The state of the s	-0.3683	0.3131	0.0234
							-0.3494	0.2370	0.0185
172 0.152 1.050	12.06	-7.5 -1.2337					and the second		
173 0.158 1.100	12.06	-7.5 -1.2489	-1,0510	-0,3897	-0.01/6	0.0240	-0.0695	0.3373	0.0238
174 0.158 1.148	12.07	-7.5 -1.2424	-1.7721	-0.3864	-0.0236	0,6145	-0.3491	0.2104	0.0266
175 0.162 1.199	12.08	-7.5 -1.2110	-1.5116	-0.4048	-0.0213	0,6284	-0.0719	0.3460	0.0263
176 0.160 0.950	14.05	-7.2 -1.4434				0.4910	-0.0755	0.3614	0.0050
177 0.152 1.000	14.05	-7.5 -1.5144	-2.3289	-0.2128	-0.0079	0.5667	-0.0823	0.3607	0.0123
178 0.170 1.049	14.07	-7.5 -1.4931					-0.0672	.0.3290	0.0108
									_
179 0.158 1.102	14.08	-7.5 -1.5180					-0.0952	0.4440	0.0185
180 0.162 1.152	14.08	-7.5 -1.5018					-0.0593	0.3016	0.0202
181 0.163 1.200	14.11	-7.5 -1.4752				0.7346	-0.1050	0.4713	0.0194
182 0.147 0.950	16.06	-7.6 -1.7089	-2,5951	-0,1382	-0.0050	0.6009	-0.0769	0.3958	-0.0036
183 0.152 1.000	16.07	-7.5 -1.5007	-2.7127	-0,1986	-0.0095	0.6803	-0.0754	0.3846	0.0026
184 0.155 1.049	16.09	-7.5 -1.7698	-2.3279	-0,3502	0.0006	0.8278	-0.3924	0.4485	0.0005
185 0.162 1.098	16.09	-7.5 -1.7873	-2.4591	-0.3790	-0.0216	0.8389	-0.0968	0.4801	0.0111
186 0.163 1.151	16.11	-7.5 -1.7858	-2.3039	-Ø,3792	-0.0260	0.8350	-0.0879	0.4333	0.0076
188 0.167 1.201	16.13	-7.5 -1.7849	-2.0205	-0.4110	-0.0236	0.8682	-0.1050	0.5001	0.0070
189 0.147 0.950	18.08	-7.6 -1.9936	-2.9534	-0.1323	-0.0071	0.7379	-0.0651	0.3478	-0.0083
190 0.154 0.999	18.09	-7.6 -2.1167	-3,0603	-0,1809	-0.0110	0.8191	-0.0741	0.4074	-0.0048
191 0.172 1.049	18.12	-7.6 -2.1202	-2.7529	-0,3743	-0.0023	1.0131	-0.0739	0.4344	-0.0032
192 0.162 1.098	18.12	-7.5 -2.1029	-2.7255	-0,3859	-0.0217	1.0004	-0.0620	0.4113	0.0052
193 0.163 1.150	18.14	-7.5 -2.1324	-2.5730	-0.3789	-0.0274	0.9982	-0.3679	0.3970	0.0001
194 0.168 1.200	18.18	-7.5 -2.1556				1.0464	-0.0874	0.4741	-0.0003
197 0.142 0.950	20.10	-7.6 -2.3252				0.9135	-0.0259	0.2214	-0.0118
198 0.149 1.001	20.13	-7.6 -2.2130	-3.2759	-0,1651	-0.0119	1.0087	-0.0693	0.3844	-0.0068
199 0.152 1.050	20.15	-7.6 -2.5289				1.1856	-0.2631	0.3984	-0.0033
200 0.154 1.098	20.16	-7.5 -2.5124	-2.9395	-0.3722	-0.0210	1.1957	-0.0971	0.4628	0.0091
201 0.157 1.149	20.18	-7.5 -2.2681				1.2089	-0.0536	0.3725	-0.0001
202 0.176 1.199	20.22	-7.6 -2.6070	-2.4425	-0.3956	-0.0215	1.2524	-0.0982	0.4652	-0.0026
203 0.145 0.949	22.14	-7.6 -2.7964					-0.0351		-0.0167
204 0.162 1.001	22.18	-7.6 -3.0235				1.2709	-0.0832		-0.0131
205 0.152 1.050	22.21	-7.6 -3.4288				_	-0.0799		-0.0097
206 0.157 1.098	22.22	-7.5 -3.0107					-0.0759		0.0043
			3,1,,1	2,0000	2.22.70		2,0,0,	2	2,2240
207 0.158 1.152	22.25	-7.5 -3.4596	-2.9432	-0,3659	-0.0241	1.4752	-0.0893	0.4321	-0.0010
208 0.162 1.198	22.29	-7.6 -3.1049			_		-0.1090		-0.0044
209 0.144 0.951	24.20	-7.6 -3.3683					-0.0323		-0.0299
210 0.149 0.999	24.24	-7.6 -3.5579					-0.0980		-0.0225
211 0.155 1.049	24.27	-7.6 -3.5918					-0.0829		-0.0174
TIT DIANA MINAN	27.27	, 10 -01-710	5.4257	2,0230	5.5557		2,002,	21,20,3	5,52,4
212 0.158 1.101	24.28	-7.6 -3.5539	-3.3986	-0,3488	-0.0229	1.7589	-0.0454	0.4182	-0.0015

TABLE 1.06

# ROLL ANGLE = -7.5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
213	0.162	1.150	24.32	-7.0	-3.6000	-3,1457	-0,3427	-0.0256	1.7720	-0.0726	0.4208	-0.0073
214	0.162	1.198	24.37	-7.0	-3.6438	-2.7818	-0.3680	-0.0199	1.8206	-0.0623	C. 4355	-0.0126
215	0.147	0.952	26.26	-7.6	-3.9124	-4.3962	-0,0400	-0.0094	1.7583	0.0138	0.3342	-0.0300
216	0.152	0.998	26.32	-7.0	-4.0712	-3.6240	-0,1112	-0.0133	1.8929	0.0227	0.3342	-0.0198
217	0.170	1.049	26.35	-7.6	-4.1258	-3.5424	-0,2958	-0.0149	2.0831	0.0075	0.3438	-0.0186
218	0.158	1.101	26.36	-7.0	-4.1203	-3.6272	-0,3375	-0.0249	2.1098	-0.0113	0.3895	-0.0111
219	0.178	1.150	26.40	-7.0	-4.1683	-3.3304	-0,3185	-0.0265	2.1152	-0.0357	3.4240	-0.0130
220	0.163	1.202	26.45	-7.0	-4.1956	-2.9154	-0,3433	-0.0224	2.1564	-0.0835	0,5269	-0.0220
221	0.147	0.950	28.32	-7.0	-4.4310	-4.1820	-0,0253	-0.0093	2.1162	0.0520	0.2661	-0.0231
222	0.152	1.001	28.40	-7.0	-4.2826	-3.5480	-0.0879	-0.0141	2.2444	0.0039	2.3966	-0.0206
223	0.155	1.049	28.42	-7.0	-4.6659	-3.6387	-0.2784	-0.0144	2.4533	-0.0261	0.4658	-0.0195
224	0.162	1.098	28.44	-7.0	-4.5775	-3.7195	-0.3160	-0.0259	2.4830	-0.0894	0.6276	-0.0214
225	0.163	1.150	28.48	-7.6	-4.7070	-3.4645	-0,2960	-0.0271	2.4811	-0.0778	0.5440	-0.0234
226	0.183	1.200	28.53	-7.6	-4.7419	-3.1373	-0,3221	-0.0214	2.5290	-0.0770	0.5402	-0.0256

TABLE 1.07

#### ROLL ANGLE = Ø DEG.

SER	REYN MA	ACH TH	HETA R	ANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
•		0.40				0 3040	-0.1557	0.0080	0.1675	a aa25	0.0169	0.0166
177	0.150 0.9			0.0	0.1125			0.0068	0.2071		-0.0033	0.0169
	0.157 1.6			0.0	0.1231		-0,1961	0.0113	0.3275		0.3244	0.0171
	0.157 1.6			0.0	0.1133		-0.3124			the second second second		-
7.1	0.160 1.	*		0.0	0.1180		-0,3574		0,3575		-0.0200	0.0169
٥	0.183 1.3	153 -2	2.02	0.0	0.1277	0.0927	-0,3396	כ/שמיש-	0.3364	0.0238	-0.0901	0,0166
7	Ø.168 1.1	199 -2	2.02	0.0	8.1485	0.1657	-0,3720	-0.0081	0.3688	-0.0090	0.0682	0.0175
8	0.150 0.9	950 -0	3.01	0.6 -	.0.0215	-0.0624	-0,1723	0.0071	0.1793	-0.0139	0.0216	0.0166
9	0.154 1.6	001 -0	0.01	0.0 -	.0.0229	-0.0725	-0,2108	0.0071	0.2178	0.0048	0.0261	0.0159
10	0.157 1.8	049 -8	8.01	0.0 -	.0,0295	-0.1035	-0,3173	0.0112	0.3284	0.0087	0.0088	0.0170
11	0.163 1.	101 -6	0.01	0.0	-0,0307	-0.1122	-0,3550	-0.0062	0.3487	0.0170	-0.0367	0.0161
12	Ø.167 1.	151 -6	0.01	u.u .	0.0247	-0.0822	-0,3514	-0.0071	0.3443	0.0072	-0.0331	0.0167
-	0.168 1.						-0,3638			-0.0102		0.0164
	0.150 0.					-0.2186		0.0035	0.1736		-0.0052	0.0172
	0.157 1.6					-0.2739		0.0050	0.2049		-0.0157	0.0166
	0.160 1.6					-0.2423		0.0102		-0.0023	The state of the s	0.0162
				•	,							
17	0.163 1.3	102 2	2.00	0.0 .	.0.1843	-0.2874	-0,3630	-0.0049	0.3643	0.0040	-0.0053	8.0178
	0.167 1.						-0,3465		0.3449	0.0150	-0.0781	0.0177
	0.168 1.2						-0.3681		0.3668	-0.0157	0.0961	0.0167
	0.150 0.9					-0.4341		0.0053	0.1965	0.0030	-0.0121	0.0200
21	0.157 1.	000	4.01	0.0	0.3528	-0.5290	-0,2054	0.0033	0.2329	0.0112	-0.0087	0.0205
22	0.160 1.6	752	4.01	α.ν.	.7.5405	-0.4730	-0.3330	7.0069	0.3635	-0.0034	0.0115	0.0204
	0.163 1.			Control of the			-0,3687	and the state of t	0.3890		0.0007	0.0210
	Ø.167 1.						-0,3510		0.3645		-0.3790	0.0207
	0.172 1.						-0,3823			-0.9083	0.0592	0.0195
	Ø.152 Ø.						-0.1623		0.2190		-0.0082	0.0235
	21252 21	,			******		-11000		-,,-			
27	0.157 1.6	000	5.02	0.0 -	.0. >537	-Ø.8717	-0,2092	-0.0004	0.2657	0.0099	-0.0385	0.0236
28	0.175 1.6	050 (	5.02	0.0 -	0.5526	-0.8009	-0,3503	0.0025	0.4088	0.0032	-0.0086	0.0240
29	0.165 1.	102					-0,3673		0,4158	0.0172	-0.0427	0.0235
30	0.167 1.	148					-0,3649		0.4076		-0.0577	0.0247
31	0,168 1,	198	6.03	0.0	-0.>312	-0.6730	-0,3954	-0.0142	0,4348	-0.0098	0.0571	0.0232
32	0.152 0.	952	8.02	0.0	-0.7281	-1.1540	-0,1625	0.0010	0.2635	0.0116	-0.0458	0.0258
	0.157 1.						-0.2081		0.3134		-0.0017	0.0263
	0.160 1.						-0,3383		0.4454	THE SECTION OF SECTION	-0.0062	0.0255
	0.165 1.6						-0,3837		0.4795		-0.0220	0.0260
100	Ø.168 1.						-0.3636		0.4491		-0.1014	0.0264
00	2,100 1,	(			-1.07/		3,0000	,	-1		5,101,	
	0.172 1.2						-0,4021		0.4845	-0.0189		0.0249
2	0.147 0.9	951 16	0.03	u.u .	0.9531	-1.5387	-0.1556	-0.0004	0.3188		-0.0712	0.0235
3	0.152 1.	000 10					-0,2030		0,3708		-0.0327	0.0258
4	Ø.155 1.6	051 18					-0,3569		0.5322		0.0142	0.0252
5	0.158 1.3	100 10	0.02	0.0	-1.0095	-1.5613	-0,3849	-0.0153	0,5395	0.0148	-0.0384	0.0258
6	0.163 1.	151 16	8.04	0.0	0.9988	-1.4987	-0,3770	-0.0204	0.5254	0.0329	-0.1169	0.0256

#### TABLE 1.07

# DATA LISTINGS

#### ROLL ANGLE = 0 DEG.

SER REYN MACH	THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
7 0.163 1.201	10.06	0.0 -0.9749	-1.2768	-0.4139	-0.0208	0.5573	-0.0076	0.0499	0.0251
8 0.147 0.950	12.04	0.0 -1.2029				0.4149		-0.0357	0.0215
9 0.152 0.998	12.04	0.0 -1.2634				0.4607		-0.0334	0.0233
10 0.157 1.050	12.05	0.0 -1.2538				0.6094		-0.0135	0.0220
11 0.175 1.098	12.05	0.0 -1.2551				0.6290		0.0010	0.0227
	16			-,					
12 0.163 1.148	12.06	Ø.0 -1.2468				0.6121		-0.0708	0.0247
13 0.167 1.200	12.08	Ø. W -1.2167					-0.0001		0.0231
14 0.163 0.952	14.05	0.0 -1.4652				0.5065		-0.0497	0.0200
15 0.154 1.000	14.05	U.U -1.7427				0.5645	0.0115	THE RESERVE OF THE PARTY OF THE	0.0191
16 0,155 1.051	14.07	D.D -1.5338	-2,2337	-0,3628	-0.0052	0.7190	0.0328	-0.0672	0.0186
17 0.160 1.102	14.07	0.8 -1.5210	-2.2275	-0.3934	-0.0208	0.7312	0.0156	-0.0268	0.0234
18 0.163 1.152	14.08	0.0 -1.5112				0.7211		-0.1018	0.0247
19 0.167 1.199	14.10	0.0 -1.4938					-0.0121		0.0259
20 0.147 0.950	16.06	0.0 -1.7388				Ø.6215		-0.0565	0.0150
21 0.154 1.001	16.07	0.0 -1.8336				0.6909		-0.0816	0.0152
									_
22 0.157 1.049	16.09	0.0 -1.8105				0.8407		-0.0908	0.0175
23 0.160 1.102	16.09	0.0 -1./959				0,8534		-0.0914	0.0221
24 0.167 1.151	16.11	0.0 -1.8016				0.8405		-0.1349	0.0200
25 Ø.167 1.199	16.13	W.W -1.7959				0.8705		-0.0242	0.0215
26 0.150 0.951	18.08	0.0 -2.0155	-3.0810	-0,1334	-0.0060	0,7466	0.0775	-0.2036	0.0176
27 0.168 1.002	18.09	U.U -2.1425	-3.1685	-0.1716	-0.0100	0.8191	0.0617	-0.1857	0.0190
28 0.158 1.948	18.12	W.W -2.1260	-2.7964	-0,3482	-0.0038	0.9886	0.3772	-0.1963	0.0200
29 0.160 1.101	18.13	W.W -2.1187	-2.7807	-0.3895	-0.0241	1.0065	0.0512	-0.1300	0.0245
30 0.180 1.149	18.14	Ø. K -2.1503	-2.6777	-0.3841	-0.0281	1.0080	0.0784	-0.2230	0.0190
31 0.168 1.199	18.18	0.0 -2.1729	-2,3486	-0,4132	-0.0234	1.0482	0.0399	-0.1024	0.0227
34 0.157 0.952	20.10	Ø. 0 -2,3617	-3 3707	-0.1149	-0.0045	0.9153	0.3567	-0.1764	0.0229
35 0.149 1.001	20.12	Ø. W -2.5640				1.0289		-0.2107	0.0220
36 0.152 1.050	20.15	0.0 -2.5741				1.2099		-0.1783	0.0244
37 0.170 1.100	20.16	Ø. b -2.5388				1.2065		-0.1409	0.0328
38 0.158 1.150	20.18	0.0 -2.5930				1.2164		-0.2434	0.0288
00 21250 21451	22.20	21- 21-700		-,		.,			
39 0.160 1.198	20.22	0.0 -2.6297	-2.5629	-0,4012	-0.0214	1.2653	0.0730	-0.1995	0.0326
40 0.145 0.950	22.14	0.6 -2.8880	-3.7229	-0.1030	-0.9970	1.1776	0.0527	-0.1714	0.0239
41 0.149 0.998	22.18	0.0 -3.0943	-3.6889	-0,1438	-0.0122	1.2902	0.0921	-0.2477	0.0252
42 0.152 1.050	22.20	0.0 -3.0967	-3.4542	-0,3562	-0.0119	1.4893	0.0895	-0.2391	0.0294
43 0.170 1.099	22.22	0.8 -3.8431	-3.3112	-0,3635	-0.0226	1.4663	0.2673	-0.2096	0.0375
44 0.158 1.151	22.25	0.0 -3.0893	-3.0897	-0.3542	-0.0223	1.4770	Ø.1392	-0.4000	0.0321
45 0.162 1.201	22.29	0.0 -3.1425				1.5331		-0.1775	0.0384
46 0.144 0.951	24.19	0.0 -3.4543				1.4791		-0.1451	0.0252
47 0.149 1.000	24.24	0.0 -3.6048				1.5825	The second second second	-0.1693	0.0256
48 0.152 1.050	24.27	0.0 -3.6224				1,7755		-0.1236	0.0293
	27.27	-,	3,7000	210512	5.5401		210204	211500	212270
49 0.155 1.100	24.28	0.0 -3.6184	-3.5559	-0,3481	-0.0209	1.7832	0.0777	-0.2240	0.0377

TABLE 1.07

#### ROLL ANGLE = Ø DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
50	0.158	1.149	24.32	0.0	-3.6533	-3,3348	-0,3308	-0.0222	1.7857	Ø.1266	-0.3817	0.0386
51	0.162	1.198	24.36	0.0	-3.6928	-2.9276	-0,3667	-0.0197	1.8396	0.0827	-0.2314	0.0362
52	0.160	0.949	26.24	0.0	-3.9674	-4.3544	-0,0429	-0.0051	1.7885	0.1528	-0.3831	0.0265
53	0.152	1.002	26.31	0.10	-4.1286	-3.7454	-0,1166	-0.0133	1.9141	0.2140	-0.4980	0.0266
54	0.152	1.048	26.34	0.0	-4.1666	-3.7817	-0,3125	-0.0130	2.1170	0.1713	-0.3634	0.0308
55	Ø.158	1.098	26.35	0.0	-4.1632	-3.8048	-0.3370	-0.0248	2,1278	Ø.1447	-0.3420	0.0369
56	0.158	1.148	26.39	0.0	-4.2021	-3.5377	-0,3132	-0.0253	2.1258	0.1517	-0.4184	0.0370
57	0.162	1.201	26.44	0.0	-4.2384	-3.1284	-0,3470	-0.0201	2.1801	0.0935	-0.2088	0.0331
58	0.147	0.950	28.31	0.0	-4.4631	-4.3824	-0,0001	-0.0094	2.1086	0.2066	-0.4339	0.0316
59	0.163	1.001	28.39	0.0	-4,6289	-3.7095	-0,0923	-0.0115	2.2682	0.0970	-0.1966	0.0288
60	0.170	1.052	28.41	0.6	-4.7004	-3.8889	-0,2996	-0.0141	2.4876	0.3611	-0.1088	0.0310
61	0.158	1.100	28.43	0.0	-4./032	-3.9123	-0,3094	-0.0233	2.4907	0.0944	-0.1975	0.0353
62	0.162	1.149	28.47	0.0	-4.7407	-3.6299	-0,2938	-0.0248	2.4966	0.3771	-0.1884	0.0324
63	0.180	1.198	28.51	0.0	-4,7768	-3.2996	-0,3255	-0.0205	2,5486	0.1288	-0.2624	0.0367

TABLE 1.08

ROLL ANGLE = 7.5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
67	0.142	0.949	-2.02	7.5	0.1115	0.0755	-0,1608	0.0070	0.1716	0.0084	0.0004	0.0168
68	0.147	0.998	-2.02	7.5	3,1215	0.1102	-0,1866	0.0059	0.1966	0.0116	-0.0110	0.0172
69	0.165	1.050	-2.02	7.5	0.1122	0.0401	-0,3147	0.0103	0.3286	0.0123	0.0097	0.0180
70	0.168	1,101	-2.02	7.5	0.1187	0.0649	-0.3543	-0.0058	0.3524	0.0133	-0.0086	0.0166
71	0.157	1.148	-2.02	7.5	0.1281	0.0883	-0,3486	-0.0107	0.3421	0.0254	-0.0683	0.0177
72	Ø.16Ø	1,199	-2.02	7.5	0.1474	0.1596	-0,3651	-0.0086	0.3614	-0.0069	0.0488	0.0172
73	0.144	0.952	-0.01	7.5	-0.0215	-0.0629	-0,1525	0.0058	0.1583	0.0094	-0.0174	0.0160
74	0.149	0,999	-0.01	7.5	-0.0264	-0.0778	-0,1974	0.0052	0.2025	0.0041	0.0140	0.0170
75	0.152	1.051	-0.01	7.5	-0.0303	-0.0988	-0,3297	0.0118	0.3414	0.0087	0.0052	0.0163
76	0.154	1.099	-0.01	7.5	-0.0310	-0.1050	-0,3550	-0.0051	0.3499	0.0183	-0.0260	0.0166
77	0.173	1.149	-0.01	7.5	-0.0261	-0.0889	-0,3409	-0.0106	0.3303	0.0234	-0.8741	0.0152
	0.162		0.01	7.5	-0.0104	-0.0081	-0,3732	-0.0088	0.3643	-0.0050	0.0629	0.0169
79	0.145	0.949	2.01	7.5	-0.1630	-0.2273	-0,1611	0.0051	0.1717	0.0081	-0.0008	0.0165
	0.149		2.00	7.5	-0.1784	-0.2707	-0,1959	0.0048	0.2067	0.0071	-0.0151	0.0170
81	0.168	1.049	2.01	7.5	-0.1777	-0.2369	-0,3129	0.0124	0.3313	0.0043	0.0118	0.0170
82	Ø.157	1.100	2.01	7.5	-0.1864	-0.2978	-0.3572	-0.0063	0.3572	0.0138	-0.0292	0.0175
	0.175		2.01				-0,3427		0.3387		-0.0924	0.0183
	Ø.162		2.01				-0.3717		0.3688	-0.3148		0.0177
85	0.144	0.951	4.01	7.5	-0.5207	-Ø.4323	-0.1660	0.0043	0.1922	0.0155	-0.0595	0.0194
86	0.149	1.002	4.01	7.5	-0.3497	-0.5152	-0,1997	0.0037	0.2273	0.0120	-0.0521	0.0200
87	0.167	1.050	4.01	7.5	-0.3473	-0.4545	-0,3361	0.0097	0.3692	0.0130	-0.0197	0.0192
	0.155		4.01	7.5	-0.5614	-0.5274	-Ø,3631	-0.0078	0.3797	0.0172	-0.0493	0.0203
	0.176		4.01				-0,3555		0.3680	0.0301	-0.1017	0.0203
90	0.162	1.199	4.01	7.5	-0.3387	-0.4012	-0,3768	-0.0107	0.3889	0.0014	0.0385	0.0201
91	0.147	0.951	6.01	7.5	-0.5051	-0.7373	-0,1578	0.0039	0.2137	0.0356	-0.1032	0.0234
92	0.152	0.999	6.01	7.5	-3.5476	-0.8447	-0.2107	-0.0004	Ø.2665	0.0368	-0.1169	0.0239
	0.167		6.02	7.5	-0.5375	-0.7311	-0,3378	0.0093	0.4016		-0.0863	0.0220
94	0.158	1.170	6.02	7.5	-0.5588	-0.8483	-0.3729	-0.0105	0.4191	0.0298	-0.1108	0.0228
95	0.162	1.152	6.02	7.5	-0.5485	-0.8003	-0.3551	-0.0139	0.3969	0.0451	-0.1706	0.0228
96	0.163	1.201	6.03	7.5	-0.5312	-0.6621	-0,3988	-0.0148	0.4376	0.0062	-0.0010	0.0218
97	0.147	0.952	8.02	7.5	-0.7192	-1.1156	-0,1668	0.0014	0.2669	0.0593	-0.1920	0.0250
98	0.163	0.999	8.02				-0.2116	-0.0017	0.3144	0.0496	-0.1851	0.0244
99	0.155	1.049	8.03	7.5	-0.7666	-1.1242	-0.3602	0.0063	0.4701	0.0351	-0.1218	0.0238
	0.158	-	8.03	-			-0,3726	-0.0138	0.4637		-0.1843	0.0246
_	0.162		8.03				-0.3733		0.4582	0.0640	-0.2431	0.0246
102	0.163	1.230	8.05	7.5	-0.7397	-0.9377	-0.4013	-0.0175	0.4835	0.9147	-0.2734	0.0227
	0.145		10.03		-0.9418			0.0000	0.3314		-0.2713	0.0259
	0.149		10.03			-	-0.2140	and the second second	0.3786	Control of the Control	-0.2593	0.0263
	0.165		10.04		-0.9935			0.0052	0.5230		-0.2208	0.0217
	0.154		10.04				-0,3779	-0.0164	0.5301	0.0745	-0.2478	0.0247
109	0.158	1.152	10.05	7.5	-0.9883	-1.4469	-0,3728	-0.0200	0.5197	0.0791	-0.3024	0.0226

TABLE 1.08

#### ROLL ANGLE . 7.5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
					2 04	4 2057	- 4 4 4 4 7		0 5440		0 4707	
	0.160		10.06			-1.2253			0.5469		-0.1303	0.0232
	0.145		12.03			-1.8742			0.4009		-0,3539	0.0284
112	0.149	0.999	12.05	7.5	-1.2494	-1.9784	-0,1998	-0.0069	0.4492	0.1034	-0.3687	0.0257
113	0.152	1.049	12.06	7.5	-1.2283	-1.7485	-0.3390	-0.0027	0.5855	0.2877	-0.3075	0.0221
	Ø.157		12.06			-1.8670			0.6284		-0.3468	0.0220
			12.20									
115	0.158	1.150	12.06	7.5	-1.2369	-1.7694	-0,3710	-0.0219	0.5999	0.1054	-0,4272	0.0228
116	0.162	1.200	12.08	7.5	-1.2029	-1.5026	-0.4002	-0.0208	0.6227	0.0758	-0.2289	0.0236
117	0.144	0.952	14.04			-2.2782			0.4886	0.1234	-0.4634	0.0316
	0.149		14.05			-2.4019			0.5533		-0.4513	0.0229
	0.152		14.07			-2.0955			9.7061		-0.4079	0.0263
114	0.132	1.000	14.07	1.0	-1.7003	-2.0977	-010762	- דעשטיע	n, / UOL	0.11/1	-0.40/7	D. DZ 03
120	0.155	1.100	14.07	7.5	-1.2150	-2.1811	-Ø.3847	-0.0192	0.7229	0.1362	-0.5021	0.0313
	0.158		14.08			-2.0764			0.7038		-0.5599	0.0253
	0.162		14.10			-1.7866			0.7386		-0.3716	0.0280
	0.147		16.06			-2,6390			0.6053		-0.6172	0.0377
124	0.149	9,798	16.07	1.5	-1.006/	-2.7356	-6,1900	-0.0092	0.6803	0.1005	-0.5563	0.0281
125	0.155	1.049	16.09	7.5	-1.7851	-2.4070	-0.3611	-0.0007	0.8411	0.1564	-0.5625	0.0320
	0.173		16.09			-2.4665			0.8431		-0.6416	0.0346
	0.162		16.10			-2.3402			0.8337		-0.7024	0.0321
	0.163		16.13			-2.0212			0.8652		-0.5458	0.0356
129	0.147	0.948	18.08	1.5	-1.9699	-2.9126	-0,1350	-0.0090	0.7311	0.1894	-0.7010	0.0503
130	0.152	1.000	18.09	7.5	-2.1132	-3.0624	-0.1653	-0.0115	0.8026	0.1988	-0.6866	0.0321
	0.170	Constitution Administration	18.12			-2.6841			Ø.9881		-0.7463	0.0421
	0.173		18.12			-2.7059			0,9967		-0.7512	0.0433
75.72	0.162	-	18.14			-2,5916			0.9895		-0.8536	0.0391
134	0.163	1,199	18.17	7.5	-2.1569	-2.2513	-0,3950	-0.0221	1.0271	0.1684	-0.6479	0.0460
137	0.145	0.950	20.10	7.5	-2.3285	-3.1995	-0.1207	-0.0067	0.9046	0.2021	-0.7034	0.0559
	0.149		20.13			-3,3052			1.0191		-0.8453	0.0423
	0.165		20.15			-2.9530			1.1795		-0.8648	0.0491
	100								-			
	0.154		20.16			-2.9170			1.1966		-0.8042	0.0547
141	0.173	1,149	20.18	1.5	-2.5709	-2.8072	-0,3590	-0.0251	1.2006	0.2058	-0.8343	0.0543
142	0.176	1 10A	20.22	7.5	-2.6045	-2,4331	-0.3923	-0.0202	1.2496	A. 1918	-0.7397	0.0608
	0.145					-3.5526			1.1376		-0.6371	0.0649
			22.14									
	0.149		22.18			-3,5349			1.2692		-0.9280	0.0579
	0.152		22.21			-3.2396			1.4527		-0.9502	0.0600
146	0,155	1.100	22.22	7.5	-3.0150	-3.1723	-0,3584	-0.0231	1.4507	0.2592	-0.9321	0.0667
147	0.158	1.150	22.25	7.5	-3.0687	-2.9692	-0.3525	-0.0240	1.4661	0.2366	-0.9264	0.0668
	0.162		22.29			-2.5825			1.5146		-0.7141	0.0778
										The second second second		0.0784
	0.160		24.20			-3.9118			1.4520		-0.8020	
	0.149		24.25			-3.5695			1.5794		-1.0376	0.0696
151	0.167	1.050	24.27	7.5	-3.6069	-3.4898	-0,3251	-0.0094	1.7707	0.2095	-0.8617	0.0691
152	0.155	1.100	24.29	7.5	-3.5881	-3.4074	-0.3511	-0.0239	1.7744	0.2447	-0.8944	0.0798
	2,2,,		-7.27		0.001		-,		**. , , ,	212111	,	

TABLE 1.08

#### ROLL ANGLE = 7.5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
	0.158	The second secon	24.33		-3.6116				1.7716	Ø.288Ø -		0.0765
154	0.178	1.198	24.37	7.5	-3.6634	-2.7805	-0,3591	-0.0221	1.8174	0.2334 -	0.8484	0.0808
155	0.145	0.949	26.25	7.5	-3.8775	-4.0126	-0,0387	-0.0116	1.7395	0.3911 -	1.2492	2.0860
156	0.149	0.999	26.32	7.5	-4.0563	-3.5676	-0.1172	-0.0163	1.8889	0.3914 -	1.3143	0.0732
157	0.155	1.052	26.35	7.5	-4.1122	-3.5758	-0,3075	-0.0190	2.0835	0.3125 -	1.0334	0.0742
158	Ø.155	1.101	26.36	7.5	-4.1319	-3.6191	-0.3205	-0.0270	2.0976	0.2678 -	0.9643	0.0865
159	0.162	1.151	26.40	7.5	-4.1690	-3.3009	-0.3235	-0.0268	2.1196	0.2863 -	1.0534	0.0831
	0.163		26.45		-4.2096				2.1732	0.2435 -	0.8654	0.0863
	0.160		28.32		-4.3698				2.0735	0.3723 -	1.1360	0.0995
	0.163	The same of the sa	28.40		-4.5697				2,2468	0.5073 -	1.5448	0.0758
163	0.178	1.049	28.42	7.5	-4,6525	-3,6280	-0,2880	-0.0208	2.4492	0.4411 -	1.3071	0.0777
164	0.158	1.098	28.44	7.5	-4.6886	-3,6930	-0,3149	-0.0284	2,4848	0.2529 -	0.8798	0.0898
165	0.162	1.150	28.48		-4.7076				2.4792	0.2671 -	0.9652	0.0928
	0.180		28.52	/25 MUSS	-4.7464	100			2,5378	Ø.2851 -		0.0901

TABLE 1.09 DATA LISTINGS

## ROLL ANGLE = 15 DEG.

SER	REYN W	ACH	THETA	RANG	VORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
2	0.145 0.	948	-2.01	15.0	0.1100	0.0881	-0,1540	0.0106	Ø.1683	0.0244	-0.3531	0.0174
	0.121 1.		-2.01	15.0	3.1196		-0.1839	0.0065	0.1944		-0.0289	0.0175
	0.155 1.		-2.02	15.0	0.1088		-Ø,3256	0.0127	0.3419	0.0047		0.0165
	Ø.158 1.		-2.02	15.0	0.1156		-0,3524		0.3518		-0.0261	0.0173
	Ø.162 1.		-2.02	15.0	3.1262		-0,3487		0.3430		-0.2616	0.0176
0	D. 102 1.	490	2.02	12.0	2.1202	0.1040	D 10407	D.10077	D.040D	2.0170	0.0010	8.2170
7	0.163 1.	199	-2.02	15.0	0.1467	0.1597	-0,3736	-0.0075	0.3709	-0.0016	0.0327	0.0171
8	0.147 0.	950	0.01	15.0	-0.0261	-0.0588	-0.1572	0.0064	0.1636	0.0099	-0.0160	0.0169
	0.152 1.		-0.01			-0.0750		0.0061	0.1968	0.0079	-0.0065	0.0168
	Ø.155 1.		-0.01			-0.0964		0.0103	0.3259	0.0084	0.0093	0.0168
	Ø.158 1.		-0.01				-0.3648		Ø.3586		-0.0087	0.0173
						_						_
13	0.178 1.	151	-0.01	15.0	-0.0305	-0.0846	-0,3477	-0.0103	Ø.3373	0.0146	-0.0595	0.0177
14	0.180 1.	200	0.01	15.0	-0.0106	-0.0097	-0.3653	-0.0080	Ø.3573	-0.0074	0.0553	0.0173
15	0.147 0.	950	2.00	15.0	-0.1667	-0.2170	-0,1634	0.0039	0.1730	0.0107	-0.0364	0.0177
16	0.152 0.	999	2.00	15.0	-7.1879	-Ø.2731	-0,1996	0.0060	0.2117	0.0192	-0.0272	0.0178
17	Ø.172 1.	049	2.01			-0.2233		0.0111	0.3339	0.0084	-0.0058	0.0162
-												
18	Ø.173 1.	099	2.00	15.0	-8.1937	-0.2985	-0,3631	-0.0013	0.3683	0.0136	-0.0333	0.0178
	0.178 1.		2.01				-0.3473		0.3464		-0.0852	0.0172
-	0.163 1.	500 (0100)	2.01				-0,3697			-0.0108		0.0181
	Ø.163 Ø.		4.01			-0,4156		0.0024	0.1840		-0.0875	0.0198
	0.152 1.					-0.5059		0.0020	0.2205		-0.0637	0.0199
~~	D. 172 1.	002	4.01	15.5	-0.5492	-0,7077	-0,1,40	0.0020	0,2203	0.02/5	-0.0037	0.0144
23	Ø.172 1.	.051	4.02	15,0	-0.3418	-0.4207	-0,3116	0.0069	0.3416	0.0115	-0.0262	0.0190
24	Ø.162 1.	098	4.02	15.0	-0.3617	-0.5255	-0,3566	-0.0049	0.3761	0.0230	-0.0771	0.0203
	0.163 1.		4.02				-0.3587		0.3717	0.0321	-0.1245	0.0205
-,-	0.180 1.		4.02				-Ø,3846			-0.0065		0.0195
	Ø.163 Ø.		6.02			-0.6972		0.0038	0.2200		-0.1424	0.0241
	Ø.152 Ø.		6.02			-0.7951		0.0036	0.2651	0.0389	-0.1746	0.0241
29	0.157 1.	049	6.03	15.0	-0.5305	-0.6763	-0,3263	0.0091	0.3892	0.0226	-0.1029	0.0203
30	Ø.162 1.	297	6.02	15.0	-3.5503	-0.8053	-0,3642	-0.0037	0.4163	0.0462	-0.1689	0.0228
31	Ø.178 1.	148	6.03	15.0	-0.5423	-0.7536	-0,3562	-0.0131	0.3982	0.0490	-0.1942	0.0224
32	Ø.183 1.	198	6.04	15.0	-0.2288	-0.6191	-0,3855	-0.0115	0.4267	0.0211	-0.0625	0.0226
	Ø.147 Ø.		8.03			-1.0409		0.0003	0.2578		-0.2753	0.0259
34	0.154 0.	999	8.03	15.0	-0.7452	-1.1213	-0.2049	0.0013	0.3082	0.0794	-0.3199	0.0256
35	0.157 1.	.051	8.04			-1.0188		0.0100	0,4468	0.0591	-0.2160	0.0220
36	0.178 1.	120	8.04	15.0	-0.7586	-1.0923	-0.3761	-0.0084	0.4701	0.0667	-0.2758	0.0250
	0.163 1.		8.04				-0,3609		0.4461	0.0797	-0.3136	0.0246
٠,					,.	.,	.,					
38	0.167 1.	198	8.05	15.0	-0.7210	-0.8553	-0,3974	-0.0164	0.4782	0.0458	-0.1650	0.0232
41	Ø.157 Ø.	950	10.03	15.0	-0.9219	-1.3875	-0,1437	0.0051	0.3071	0.1057	-0.4136	0.0283
42	0.145 1.	000	10.04	15.0	-0.9700	-1.4589	-0,2022	-0.0007	0.3674	0.1093	-0.4510	0.0268
	0.165 1.		10.05	15.0	-0.9650	-1.3194	-0,3402	0.0079	0.5111	0.0933	-0.3474	0.0241
44	0.154 1.	131	10.04				-0,3745	-0.0120	0.5267	0.1037	-0.4074	0.0245
45	0.157 1.	149	10.05	15.0	-0.9677	-1.3472	-0,3662	-0.0170	0.5126	0.1193	-0.4447	0.0244

### TABLE 1.09

### DATA LISTINGS

### ROLL ANGLE = 15 DEG.

SER	REYN	MACH	THETA	RANG	JAMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
				45 0	4 0		-0 4050	0 0177	0 5457	0 0747	9 2754	0.0240
	0.160		10.06		-0.9375				0.5457		-0.2751	
	0.142		12.04		-1.1565				0.3986		-0.6249	0.0325
	0.162		12.04		-1.2163				0.4417	A CONTRACTOR OF THE PARTY OF TH	-0.6575	0.0276
	0.150		12.06		-1.2025				0.5950	_	-0.5078	0.0265
50	0.154	1.130	12.06	15.6	-1.2192	-1.7238	-0,3785	-0.0188	0,6064	0.1694	-0.6250	0.0288
51	0.172	1.148	12.06	15.0	-1.2130	-1.6423	-0,3717	-0.0187	0.5987		-0.7088	0.0278
	0.162		12.08		-1.1791				0,6297		-0.5052	0.0295
	0.142		14.05		-1.4018				0.4732		-0.7907	0.0397
	0.149		14.06		-1.4780				0.5387		-0.8295	0.0308
55	0.152	1.051	14.07	15.0	-1.4624	-1.9182	-0,3647	-0.0010	0.7084	Ø.1962	-0.7322	0.0347
56	0.154	1.099	14.07	15.0	-1.4710	-2.0059	-0.3781	-0.0153	0.7096	0.2244	-0.8523	0.0352
	0.157		14.09		-1.4646				0.6976	0.2257	-0.9273	0.0350
	0.162		14.10		-1.4295				0.7278	0.1845	-0.6840	0.0342
	0.157		16.07		-1.6541				0.5832		-0.9053	0.0511
	0.162		16.08		-1.7469				0.6495		-0.9447	0.0374
-					•			_				
61	0.168	1.048	16.10	15.0	-1.7186	-2.1175	-0,3486	0.0012	0.8128	0.2420	-0.8397	0.0439
62	0.155	1.101	16.10	15.0	-1.7351	-2.2302	-0,3750	-0.0146	0.8274	0.2646	-1.0270	0.0445
63	0.157	1.148	16.11	15.0	-1.7441	-2.1219	-0.3707	-0.0191	0.8218	0.2796	-1.0673	0.0419
64	0.162	1.230	16.14	15.0	-1.7350	-1.7966	-0.4069	-0.0184	0.8554	0.2221	-0.8375	0.0421
65	0.144	0.951	18.08	15. K	-1.9240	-2.6786	-0.1245	-0.0159	0,7005	0.2459	-0.9129	0.0659
66	0.163	1.020	18.10	15.0	-2.0621	-2.7920	-0.1801	-0.0109	0.8014	0.2674	-1.0317	0.0433
100000	0.168		18.13		-2.0262				0.9459		-0.9318	0.0520
	0.155		18.14		-2.0598				0.9895		-1.1069	0.0539
	0.158		18.15		-2.0890				0.9857		-1.1562	0.0486
	0.162		18.19		-2.1065				1,0125		-0.9967	0.0572
_	0.145	Control of the Contro	20.11		-2.2942	200			0,9013	Diane Television and Inches	-0.8240	0.0804
	0.149		20.14		-2.4602				0,9909		-1,1263	0.0626
_	0.152		20.17		-2.4584				1.1596		-1.0331	0.0672
	0.157		20.18		-2.4588				1.1844		-1.2186	0.0652
75	0.158	1.148	20.21	15.0	-2.5223	-2.5634	-0,3492	-0.0180	1.1818	0.3039	-1.2201	0.0636
76	2.162	1,198	20.25	15.0	-2.5582	-2.1711	-0,3806	-0.0169	1,2264	0.2575	-1.0081	0.0747
	0.144		22.15		-2./948				1.1365	0.2179	-0.8361	0.0945
	0.162		22.19		-2.9984				1.2619		-1.3044	0.0772
	0.165		22.22		-2.9853				1.4140		-1.2333	0.0844
	0.170		22.23		-2.9663				1.4307		-1.1776	0.0844
-	-,-,-		22.20				-,					
6	0.157	1.152	22.27		-3.0334				1.4447	0.2933	-1.1995	0.0819
7	0.160	1.198	22.31	15.0	-3.0569	-2.2751	-0,3727	-0.0218	1.4849	0.2499	-0.9809	0.0920
8	0.142	0.950	24.21	15.0	-3.5147	-3.4127	-0,0774	-0.0168	1.4148	0.2442	-1.0035	0.1115
9	0.149	0.999	24.26	15.0	-3.4733	-3.1499	-0,1299	-0.0159	1.5310	0.3620	-1.4240	0.0987
10	0.150	1.048	24.29	15.6	-3.4874	-2.9249	-0,3096	-0.0082	1.7092	0.3251	-1.2809	0.1048
11	0.170	1.100	24.30	15.0	-3.2367	-3.1060	-0,3381	-0.0197	1.7457	0.2957	-1.2062	0.1000
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TABLE 1.09

## ROLL ANGLE = 15 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
12	0.173	1.151	24.33	15.0	-3.2667	-2.8425	-0,3316	-0.0302	1.7444	0.3265	-1.3135	0.0943
13	0.162	1.272	24.38	15.0	-3.6039	-2.4544	-0,3594	-0.0239	1,7920	0.2907	-1.1016	0.1023
14	0.142	0.950	26.27	15.0	-3./439	-3.4479	-0,0613	-0.0228	1.6913	0.3133	-1.1810	0.1213
15	0.149	1.002	26.32	15.0	-3.9199	-3.0610	-0,1158	-0.0205	1.8238	0.4751	-1.6832	0.1085
16	0.152	1.048	26.36	15.0	-3.9988	-3.0574	-0,3071	-0.0140	2,0377	0.4187	-1.4792	0.1189
17	0.155	1.132	26.37	15.0	-4.0475	-3.2462	-0,3232	-0.0303	2,0601	0,3978	-1.3908	0.1088
18	0.158	1.151	26.41	15.0	-4.1055	-3.0017	-Ø,3173	-0.0276	2.0855	0.2957	-1.2507	0.1059
19	0.162	1.200	26.45	15.0	-4.1555	-2.6830	-0,3431	-0.0267	2.1346	0.2956	-1.1095	0.1082
20	0.145	0.948	28.34	15.0	-4.2487	-3.3815	-0,0286	-0.0162	2.0274	0.3749	-1.2955	0.1355
21	0.149	0.998	28.41	15.0	-4.4484	-3.0214	-0,1017	-0.0191	2,1884	0.5414	-1.8435	0.1168
22	0.152	1.049	28.42	15.0	-4.2519	-3.1846	-0,2883	-0.0181	2.4045	0.4496	-1.5402	0.1279
23	0,157	1.098	28.45	15.0	-4,6081	-3.3846	-0,3159	-0.0241	2.4513	0.4031	-1.4312	0.1195
24	0.175	1.151	28.48	15.0	-4.6352	-3.1718	-0,2835	-0.0298	2.4334	0.4034	-1.4633	0.1135
25	0,162	1.198	28.53	15.0	-4,6916	-2.8438	-0,3201	-M.0254	2.4997	0.3051	-1.0779	0.1140

TABLE 1.10 DATA LISTINGS

ROLL ANGLE = 22,5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	M WAY	ROLL M
_		3 054		20 -	4 4057	2 4222	-0 45/4	0.0059	0 4450		2 2040	2 24 20
	0.139		-2.01	22.5	0.1053		-0,1564		0.1658		-0.0219	0.0179
	0.158		-2.02	22.5	0.1101		-0.1723	0.0049	0.1808		-0,0065	0.0172
	0.147		-2.02	22.5	8.1101		-Ø,32ØØ	0.0043	0.3279		0.0093	0.0187
	0.165		-2.02	22.5	3.1139		-0,3528		0.3495		-0.0275	0.0182
6	0.155	1.149	-2.01	22.5	0.1242	0.1017	-0,3460	-0.0080	0.3422	0.0237	-0.0781	0.0171
7	0.157	1.200	-2.02	22.5	0.1451	0.1605	-0,3690	-0.0086	0.3652	-0.2028	0.0335	0.0186
8	0.142	0.951	0.01	22.5	-0.0235	-0.0554	-0,1559	0.0058	0.1617	0.0215	-0.0322	0.0174
9	0.145	1.000	0.00	22.5	-0.0306	-0.0674	-0.1928	0.0055	0.1982	0.0013	-0.0035	0.0164
10	0.150	1.049	-0.01	22.5	-0.0288	-0.0883	-0.3104	0.0112	0.3215	0.0070	-0.2078	0.0165
	0.154		-0.01				-0,3506	-0.0045	0.3461		-0.0026	0.0161
							-,					
12	0.155	1.148	-0.01	22.5	-0.0321	-0.0813	-0.3594	-0.0107	0.3487	0.0153	-0.0659	0.0181
	0.157		0.01				-0.3700		Charles of the control of the control of		0.0433	0.0168
	0.142		2.00			-0.2084		0.0062	Ø.1722		-0.0222	0.0165
	0.147		2.00	22.5	-0 1821	-0.2573	-0 1004	0.0055	0.1997		-0.0431	0.0181
											_	
10	0.150	1.040	2.00	22.5	-0.1/58	-0.2179	-0,3099	0.0131	0.3289	0.0059	0.0067	0.0171
	2 151	4 4 4 4 4	2 44	22 5	4 1000	9 2066	-0 7447	0 4047	7445	0.0400		2 2404
	0.154	100	2.00				-0,3463		0.3465		-0.0329	0.0184
	0.157		2.00				-0,3544		0.3509		-0.0752	0.0183
	0.160		2.01				-0,3650			-0.0008		0.0180
	0.142		4.00			-0.3855		0.0025	0.1956		-0.0788	0.0199
21	0.162	1.001	4.00	22.5	-0.3439	-0.4759	-0.2016	0.0030	0.2282	0.0274	-0.0746	0.0196
	0.150		4.01			-0.3480		0.0055	0.3364		-0.0305	0.0180
23	0.154	1.099	4.01	22.5	-8.3565	-0.5000	-0,3596	-0.0063	0.3774	0.0292	-0.0657	0.0198
24	0.173	1.151	4.02	22.5	-0.3492	-0.4656	-0,3483	-0.0120	0.3599	0.0271	-0.1294	0.0204
25	0.175	1.202	4.01	22.5	-0.5312	-0.3601	-0,3781	-0.0101	0.3902	0.0084	-0.0037	0.0190
28	0.157	0,949	6.02	22.5	-0.4800	-0.6208	-0,1583	0.0036	0,2113	0.7465	-0.1821	0.0229
29	0.145	1.000	6.02	22.5	-0.5184	-0.7274	-0,1945	0.0010	0.2488	0.0504	-0.1632	0.0236
30	0.150	1.050	6.02	22.5	-0.5124	-0.6262	-0.3357	0.0095	0.3970	0.0438	-0.1187	0.0192
31	0.154	1.101	6.02	22.5	-0.5311	-0.7376	-0,3596	-0.0063	0.4071	0.0575	-0.1598	0.0219
-	0.157		6.02				-0,3513		0.3930		-0.2373	0.0213
	0.160		6.03				-0,3852		0.4250		-0.0578	0.0209
••							-,,,,,,					
34	0.142	0.951	8.03	22.5	-0.6724	-0.9155	-0,1501	0.0010	0.2435	0.0851	-0.3148	0.0259
	0.147		8.03				-0.1998		0.2960		-0.3232	0.0247
	0.150		8.04			-0.8118		0.0065	0.4045		-0.2349	0.0214
	0.154		8.04				-0,3713				-2.3179	0.0238
									Ø.4617	The same of the sa	the state of the s	Control of the Contro
38	0.157	1.150	8.04	22.5	-0./144	-0.9250	-0,3590	-0.0132	0,4422	0.0995	-0.3730	0.0233
70	a 174	1 100	0 05	22 5	-4 6005	-0 7444	-0 7050	-0.0174	0 4455	0 0540	-8 1007	9 9349
	0.176		8.05				-0,3859		0.4655		-0.1827	0.0218
	0.142		10.03				-0.1536		0.3033		-0.4798	0.0269
	0.162		10.03				-0,2006		0.3579		-0.4877	0.0256
	0.167		10.05			-1.1630		0.0045	0.5017		-0.4006	0.0232
43	0.157	1.098	10.05	22.5	-0.9291	-1.2228	-0,3737	-0.0109	0.5193	0.1403	-0.4790	0.0256
44	0.157	1,148	10.06	22.5	-4.9292	-1.1848	-0,3667	-0.0158	0,5076	0.1342	-0.5194	0.0242

TABLE 1.10

## ROLL ANGLE = 22,5 DEG.

SER	REYN M	ACH TH	ETA F	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
45	0.176 1.	100 10	.07 2	22 5	-7 4004	-0 9457	-0,3922	-0.0164	0.5271	0 0851	-0.3074	0.0225
							-0.1490		0.3727		-0.6925	0.0304
	0.144 0.									-		
	0.149 1.						-0,1950		0.4300		-0.7352	0.0276
	0.152 1.						-0,3537		0.5939		-0.6058	0.0268
49	0.157 1.	098 12	.07 2	22.5	-1.1608	-1.4809	-0,3838	-0.0136	0.6046	0.1874	-0,7003	0,0279
	Ø.158 1.						-0,3728		0.5903		-0.7141	0.0281
	0.162 1.3						-0,3953		0.6057		-0.5002	0.0289
52	0.144 0.9	951 14	.06 2	22.5	-1.3367	-1.8107	-0.1445	-0.0036	0,4614	0.2400	-0.8647	0.0385
53	0.149 0.	998 14					-0,1903	-0.0048	0.5207	0.2578	-0.9501	0.0318
54	0.152 1.	048 14	.09 2	22.5	-1.3970	-1.6321	-0,3312	0.0061	0.6671	0.1976	-0.7249	0.0349
55	0.155 1.3	101 14	.09 2	22.5	-1.4075	-1.7283	-0,3698	-0.0135	0.6881	0.2292	-0.8825	0.0356
56	0.158 1.3	149 14	.09 2	22.5	-1.4046	-1.6375	-0,3769	-0.0192	0.6890	0.2364	-0.9583	0.0367
57	0.178 1.3	202 14	.11 2	22.5	-1.3823	-1.3567	-0,4112	-0.0179	0.7185	0.1936	-0.7447	0.0390
58	0.147 0.9	952 16	.07 2	22.5	-1.5798	-2.0940	-0,1368	-0.0057	0.5634	0.2629	-0.9313	0.0529
59	0.163 1.						-0,1791		0,6288	0.2987	-1.0785	0.0403
60	0.152 1.	849 16	.12 2	2.5	-1.6519	-1.8306	-0,3460	0.0028	0.7935	0.2453	-0.8851	0.0467
	Ø.157 1.		.11 2	2 5	-1.6651	-1.9452	-0,3681	-0.0153	0.8009		-1.0658	0.0455
	Ø.158 1.						-0,3665		0.7970		-1.1293	0.0455
_	0.163 1.						-0,3954		0.8266	-	-0.8975	0.0524
	Ø.139 Ø.						-0,1230		0.6862		-0.9196	0.0724
00	D,13, D,	200 10	,		-110332	-2.0/20	6,1230		D.0002	0,2327	-0,7170	0.0724
67	Ø.144 Ø.	998 18	.10 2	22.5	-1.9792	-2.4516	-0,1583	-0.0120	0.7541	0.2825	-1.0766	0.0536
68	0.147 1.	050 18	.13 2	22.5	-1.9667	-2.0534	-0,3364	-0.0010	0.9308	0.2523	-0.9125	0.0610
69	Ø.152 1.	099 18	.14 2	22.5	-1.9720	-2.1508	-0,3572	-0.0185	0.9356	0.2990	-1.1460	0.0618
70	0.154 1.	151 18	.16 2	22.5	-2.0145	-2.0092	-0,3491	-0.0232	0.9373	0.3016	-1.2233	0.0581
71	0.157 1.3	201 18	.19 2	22.5	-2.0365	-1.6929	-0,3918	-0.0189	0.9899	0.2517	-0.9694	0.0659
7.0					2 2222							~ ~~~
_	0.142 0.						-0.1206		0.8686		-0.9391	0.0879
_	0.147 0.						-0.1609		0.9567		-1.1750	0.0678
	0.150 1.						-0,3404		1.1400		-0.9820	0.0746
	0.154 1.						-0,3551		1.1427		-1.1268	0.0756
76	0.157 1.	152 20	1.21 2	22.5	-2.4506	-2.1913	-0,3634	-0.0245	1.1646	0.3043	-1.2059	0.0738
77	0.157 1.	198 20	1.24 2	2.5	-2.4800	-1.8375	-0,3836	-0.0193	1.2032	0.2322	-0.9171	0.0809
	0.142 0.		.17	22.5	-2.7012	-2.7719	-0.1032	-0.0128	1.1030		-1.0469	0.1023
	0.145 1.						-0,1499		1.2129		-1.3216	0.0874
	0.150 1.						-0.3104		1.3663		-1.0863	0.0956
-	0.154 1.						-0,3460		1.3994		-1.1969	0.0892
01	D.134 1.	24, 22	25	22.5	-2.7629	-2.5104	-0,3400	-0.0214	1,3994	0.3020	-1.1909	0.0072
82	0.157 1.3	150 22	.27 2	22.5	-2.9413	-2.3117	-0,3529	-0.0226	1.4205	0.3099	-1.2132	0.0838
83	0.160 1.3	202 22	.31 2	22.5	-2.9775	-1.9319	-0,3769	-0.0221	1,4590	0.2563	-0,9997	0.0928
84	0.142 0.	950 24	.23 2	22.5	-3.1816	-2.8372	-0,0783	-0.0157	1.3627	0.3718	-1.3079	0.1157
	0.145 1.						-0.1305		1.4842		-1.5628	0.1035
	Ø.165 1.						-0,3073		1.6541		-1.2045	0.1153
87	0.154 1.5	099 24	.32 2	22.5	-3,4312	-2.6849	-0,3405	-0.0247	1.7005	0.3316	-1.2790	0.1052
				and and								

TABLE 1.10

# ROLL ANGLE = 22,5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F YAW M	ROLL M
88	0.157	1.149	24.35	22.5	-3.4751	-2.4773	-0,3332	-0.0279	1.7108	0.3479 -1.2746	0.0949
89	0.160	1.200	24.39	22.5	-3,5123	-2.1096	-0,3561	-0.0228	1.7540	0.2883 -1.0376	0.0965
90	0.142	0.952	26.28	22.5	-3,5912	-2.8257	-0.0501	-0.0181	1.6189	0,4200 -1,4225	0.1339
91	0.145	1.000	26.34	22.5	-3.7931	-2.6279	-0.1072	-0.0205	1.7684	0.4711 -1.6986	0.1172
	0.168		26.37		-3.8840				1,9859	0.3446 -1.2582	0.1264
93	0.155	1.100	26.38	22.5	-3.9477	-2.8690	-0.3236	-0.0294	2.0175	0.3470 -1.2943	0.1143
94	Ø.173	1.150	26.42		-3.9987				2.0321	0.3904 -1.4146	0.1033
	Ø.176		26.47		-4.0484				2.0826	0.2973 -1.0599	0.1044
96	Ø.144	0.952	28.35		-4.0847				1.9415	0.4506 -1.4358	0.1469
10 to	0.162		28.42	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	-4,5378				2,1187	0.5347 -1.8368	0.1241
98	Ø.152	1.049	28.45	22.5	-4.4303	-2.6542	-0,2812	-0.0277	2.3332	0.4341 -1.4801	0.1303
99	0.155	1.100	28.46	22.5	-4.5027	-2.9468	-0,3257	-0.0323	2,4035	0,4238 -1.4564	0.1194
100	Ø.158	1.151	28.50	22.5	-4,5473	-2.7596	-0.2900	-0.0328	2.3955	0.4028 -1.4480	0.1127
	0.175		28.54		-4.6132				2.4660	0.2914 -1.0316	0,1138

TABLE 1.11
DATA LISTINGS

## ROLL ANGLE = 30 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
41	0.147	0 940	-2.01	30.0	0.1145	0 0851	-0,1541	0.0098	0.1678	0.0131	-0.0155	0.0180
	0.152		-2.01	30.0	0.1211		-0,1835	0.0065	0.1941	-	-0.0192	0,0185
	0.157		-2.02	30.0	0.1074		-0,2972	0.0147	0,3154		0.0236	0.0175
	0.160		-2.02	30.0	0.1204		-0,3589		0.3609		-0.0195	0.0172
	0.167		-2.02	30.0	0.1313		-0,3540		0.3511		-0.0586	0.0181
			-2.02	30.0	0,1313	0,1227	-610246		0.0011	0,0200	-6.6500	0.0101
	0.168		-2.02	30.0			-0,3637	-0.0070	0.3619	0.0052		0.0176
	0.150		-0.01		-0.0216			0.0054	0.1657		-0.0221	0.0167
	0.154		-0.09	-0.1	-0.0240	-0.0599	-0,1815	0.0085		-0,0011		0.0176
	0.157		-0.01		-0.0162			0.0116	0.3151		-0.0180	0.0151
50	Ø,163	1.102	-0.01	30.0	-0.0290	-0.1014	-0,3583	-0.0044	0.3539	0.0178	-0.0366	0.0178
51	0.167	1.151	-0.01	30.0	-0.0177	-0.0557	-0,3537	-0.0045	0.3491	0.0179	-0.0422	0.0176
53	0.168	1.199	0.01	30.0	-0.0044	0.0014	-0,3635	-0.0083	0.3551	-0.0036	0.0342	0.0176
54	0.150	0.950	2.00	30.0	-0.1557	-0.1855	-0,1557	0.0082	0.1692	0.0135	-0.0481	0.0180
55	0.157	1.003	2.00	30.0	-0.1721	-0,2424	-0,1804	0.0073	0,1935	0.0119	-0.0350	0.0180
56	0.162	1.052	2.01	30.0	-0.1584	-0,1741	-0,3126	0.0060	0.3239	0.0113	-0.0067	0.0165
57	0.165	1.102	2.00	30.0	-0.1838	-8.2768	-0.3507	0.0054	0.3623	0.0183	-0.0337	0.0175
	Ø.168		2.00				-0,3477		0.3449		-0.0786	0.0189
	0.172		2.01				-0,3602			-0.0048		0.0181
	0.155		4.01	30.0	-0,2983	-0.3499	-0.1606	0.0052	0.1863		-0.0849	0.0189
	Ø.158		4.01		-0.3282			0.0063	0,2139		-0,0729	0.0199
				7 - 15 4					-			
5.00	0.162	* 110	4.02		-0.3113		54 90 00 00 000	0.0126	0,3345		-0,0254	0.0169
	0.168		4.01				-0,3574		0,3753		-0.0656	0.0199
	0.173		4.02				-0,3513		0.3661		-0.1137	0.0203
	0.176		4.02				-0,3611		0.3733		-0.0007	0.0185
66	0.155	0.949	6.02	30.0	-0,4634	-0,5616	-0,1417	0.0045	0.1940	0.0438	-0.1566	0.0236
67	0.158	0,999	6.02	30.0	-0.4958	-0.6523	-0,1939	0.0056	0.2503	0.0443	-0.1689	0.0240
68	0.165	1.050	6.03	30.0	-0.4745	-0.4753	-0,3178	0.0125	0.3783	0.0262	-0.0816	0.0182
69	0.168	1.102	6.02	30.0	-0.5118	-0.6492	-0,3553	-0.0060	0.4011	0.0382	-0.1590	0.0231
70	0.173	1.150	6.03	30.0	-0.5083	-Ø.6229	-0,3547	-0.0112	0,3950	0.0464	-0.1878	0.0224
71	0.175	1.202	6.03	30.0	-0.4826	-0.4768	-0,3802	-0.0083	0.4205	0.0148	-0.0460	0,0205
70	Ø.155		8.03	30 0	-0,6351	-0 7940	-0 4500	0.0038	0.2489	0 0404	-0.2572	0.0267
	Ø.162		8.03		-0.6696			0.0035	0.2870		-0.2608	0.0260
	Ø.165		8.04		-0.6806			0.0136	0.4234		-0.1796	0.0233
	0.170		8.04				-0.3657		0.4508		-0.2597	0.0237
	Ø.173										-0.2577	0.0254
/0	D.1/3	1,149	8.05	30,0	-0,0903	-0.0072	-0,3640	-6.0145	0,4427	B.0034	-6.2012	0.0254
77	Ø.178	1.199	8.06	30.0	-0.6542	-0.6170	-0,3853	-0.0123	0.4610		-0.1197	0.0231
80	0.147	0.948	18.04	30.0	-0.8307	-1.0284	-0,1373	0.0074	0.2872	0.0969	-0.3739	0.0280
81	0.152	1.002	10.04		-0,8785			0.0027	0.3382	0.1104	-0.3992	0.0257
	0.155		10.05	30.0	-0.8535	-0.8596	-0,3031	0.0105	0.4578	0.0941	-0.3099	0.0250
83	0.158	1.099	10.05	30.0	-0.8863	-1.0416	-0.3679	-0.0095	0.5076	0.1019	-0.3863	0.0257
84	0.163	1.151	10.06	30.0	-0.8948	-1.0291	-0,3609	-0.0139	0.4979	0.0948	-0.3967	0.0253
		-				-						

TABLE 1.11
DATA LISTINGS

ROLL ANGLE = 30 DEG.

						•				
SER	REYN MACH	THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
85	0.167 1.198	10.07	30.0 -0.8615	-0 8031	-0.1907	-0.0140	0.5207	0.0404	-0.1926	0.0231
	0.147 0.949	12.05	30.0 -1.0413			0.0025	0.3570		-0.5495	0.0292
	0.152 0.998	12.05	30.0 -1.1031			0.0041	0.4228		-0.6116	0.0259
	0.157 1.049	12.07	30.0 -1.0836			0.0117	0.5541		-0.4369	0.0247
	0.162 1.099	12.07	30.0 -1.1092	-1.2848	-0.3675		0.5822		-0.5247	0.0251
	01102 11-77		21.1072		0,00,2		.,,,,,	0.1.00	.,,,,,	210272
90	0.167 1.149	12.08	30.0 -1.1162	-1.2520	-0,3689	-0.0132	0,5813	0,1465	-0.5747	0.0279
91	0.168 1.198	12.09	30.0 -1.0885	-1.0091	-0,3990	-0.0142	0.6043	0.1034	-0.3716	0,0280
	0.150 0.954	14.06	30.0 -1.2751			0.0007	0.4447		-0.6880	0.0319
	0.154 0.998	14.08	30.0 -1.3439				0.4967		-0.7724	0.0291
95	0.158 1.048	14.10	30.0 -1.2741	-1.1366	-0,2887	0.0055	0,5957	0.1751	-0.6058	0.0241
96	0.163 1.099	14.09	30.0 -1.3516	-1.5151	-0.3699	-0.0118	0.6764	0.1746	-0.6756	0.0307
	0.167 1.150	14.10	30.0 -1.3530		The state of the s		0.6629		-0.7447	0.0335
	0.168 1.199	14.12	30,8 -1,5227				0.6850		-0.5363	0.0340
	0.150 0.950	16.08	30.0 -1.5092				0.5404		-0.7785	0.0420
100	0.154 0.999	16.09	30.0 -1.6047	-1.9557	-0,1578	-0.0028	0.5937	0.2348	-0.8964	0.0339
	0.160 1.049	16.12	30.0 -1.5751			0.0083	0.7511		-0.7279	0.0404
	0.163 1.098	16.12	30.0 -1.6095				0.7870		-0.8816	0.0395
	0.168 1.150	16.13	30.0 -1.6139				0.7802		-0.9351	0.0445
A CONTRACTOR OF THE PARTY OF TH	0.172 1.199	16.16	30.1 -1.2941				0.7958		-0.7531	0.0459
105	0.152 0.948	18.10	30.0 -1.7602	-2.0586	-0,1261	-0.0050	0.6620	0.2297	-0.8457	0.0608
106	0.157 1.001	18.12	30.0 -1.8957	-2.1673	-0.1641	-0.0071	0.7388	0.2413	-0.9139	0.0464
-	9.163 1.049	18.15	30.0 -1.8293				0.8798		-0.7879	0.0530
108	0.165 1.100	18.16	30.4 -1.8941				0.9141		-1.0227	0.0525
109	0.168 1.149	18.17	30.0 -1.9347	-1.7341	-0,3590	-0.0222	0.9234	0.2634	-1.0010	0.0545
110	0.173 1.199	18.20	30.0 -1.9564	-1.3858	-0,3895	-0.0172	0.9650	0.2274	-0.8563	0.0542
			70 2							
	0.145 0.948	20.12	30.0 -2.0884				0.8271		-0.9801	0,0744
	0.152 1.000	20.15	30.0 -2.2685				0,9140		-0.9560	0.0643
	0.155 1.052 0.158 1.098	20.18	30.0 -2.2717				1.0930		-0.7711 -0.9184	0.0729
	0.162 1.150	20.21	30.0 -2.3551				1.1232		-1.0344	0.0663
11,	D.102 1.130	20.21	30.2 -2.3331	1.,102	0,000,	-0.0240	1.1202	6.2047	-1.0344	0.0000
118	0.167 1.200	20.25	30.0 -2.3943	-1.4993	-0.3812	-0.0176	1.1700	0.1865	-0.7686	0.0724
119	0.147 0.949	22.17	30.0 -2.5265				1.0419		-0.9136	0.0918
120	0.152 0.999	22.21	30.0 -2.7375				1.1499		-1.0388	0.0768
121	0.157 1.050	22.25	30.0 -2.6979	-1.7545	-0,3088	-0.0112	1.2972	0.2069	-0.8329	0.0793
122	0.160 1.099	22.24	30.0 -2.7792	-2.2182	-0,3578	-0.0214	1.3632	0.2344	-0.9213	0.0790
107	0 147 1 149	22.20	70 W - 2 HEAD	2 2554	-0 7470	-0.0045	4 7700	a 2577	-4 7440	2 2744
	Ø.163 1.148 Ø.167 1.198	22.28	30.0 -2.8529 30.0 -2.8701				1.3789		-1.0162	0.0766 0.0759
	0.150 0.951	24.23	30.0 -2.9779				1.2926		-1.0905	0.0982
	0.154 1.001	24.27	30.0 -3.2178				1.4265		-1.2562	0.0894
	0.157 1.051	24.31	30.0 -3.2428				1.6087		-0.9431	0.0943
				-,-,,	.,,			- 12		
128	0.162 1.099	24.31	30.0 -3.3158	-2.3600	-0,3376	-0.0246	1.6507	0.2545	-0.9837	0.0876

TABLE 1.11

## ROLL ANGLE = 30 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	M WAY	ROLL M
129	0.167	1.148	24.35	30.0	-3.3763	-2.1841	-0,3192	-0.0286	1.6570	Ø.2856	-1.0390	0.0856
130	0.168	1.198	24.40	30.0	-3.4165	-1.7480	-0,3502	-0.0225	1.7100	0.2552	-0.8764	0.0804
131	0.150	0.948	26.29	30.0	-3.4583	-2.3807	-0,0641	-0.0123	1.5782	0.2542	-1.0635	0.1201
132	0.157	0.997	26.35	30.0	-3,/195	-2.3232	-0,0947	-0.0157	1.7215	0.3030	-1.2734	0.1027
133	0.158	1.048	26.39	30.0	-3.7699	-2.0793	-0,2913	-0.0159	1.9223	0.2597	-1.0293	0.1041
134	Ø.163	1.099	26.39	30.0	-3.8727	-2.5277	-0,3218	-0.0244	1.9880	0.2414	-0.9853	0.0953
135	0.167	1.149	26.43	30.0	-3,9131	-2.3391	-0,3102	-0.0305	1,9922	0.2731	-1.0742	0.0919
136	0.172	1.200	26.48	30.0	-3.9606	-1.9333	-0,3335	-0.0254	2.0418	0.2350	-0.8592	0.0895
137	0.150	0.949	28.36	30.0	-3.9892	-2.3896	-0,0256	-0.0187	1.9011	0.2412	-1.0263	0.1319
138	0.157	1.002	28.43	30.0	-4.2258	-2.1983	-0,0894	-0.0199	2.0728	0.3431	-1.3152	0.1089
139	0.162	1.051	28.46	30.0	-4.3583	-2.3300	-0.2831	-0.0141	2.3135	Ø.2781	-1.0426	0.1026
140	0.163	1,100	28.47	30.0	-4.4248	-2.6157	-0,3141	-0.0312	2.3582	0.2716	-1.0513	0.0985
141	0.168	1.150	28.50	30.0	-4.4767	-2.4792	-0,2946	-0.0326	2.3670	0.3015	-1.1401	0.0983
142	0.173	1.200	28.56	30.0	-4.5111	-2.1128	-0,3154	-0.0283	2,4088	0.2293	-0.8521	0.0937

TABLE 1.12 DATA LISTINGS

ROLL ANGLE = 37,5 DEG.

SER	REYN MACH	THETA	RANG JORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
2	0.152 0.949	-2.02	37.5 0.1148	0.0821	-0.1647	0.0099	0.1785	0.0192	-0.0364	0.0174
_	0.158 1.002	-2.02	37.5 0.1187		-0,1964		0.2060		-0.2239	0.0176
	0.162 1.049	-2.02	37.5 7.1206		-0.3302	0.0111	0.3452		-0.0117	0.0179
	0.165 1.130	-2.02	37.5 0.1185		-0,3496		0.3472		-0.0199	0.0178
	0.172 1.149		37.5 0.1282		-0,3478		0.3421		-0.0965	0.0169
0	0.1/2 1.147	-2.02	37.3 0.1232	0,0,77	D,0470	-0.0077	D,0421	0.0250	0,0,0,	0.010
7	0.173 1.201	-2.02	37.5 2.1492		-0,3725	-0.0076	0.3699	-0.0067	0.0440	0.0180
8	0.155 0.951	0.01	37.5 -0.0184	-0.0421	-0,1542	0.0062	0.1603	0.0136	-0.0280	0.0163
9	0.158 1.002	0.01	37.5 -7.0257	-0.0639	-0,1981	0.0049	0.2029		-0.0235	0.0167
10	0.165 1.050	-0.01	37.5 -3.0307	-0.0870	-0,3311	0.0124	0.3435	0.0099	-0.0136	0.0166
11	0.168 1.099	-0.01	37.5 -2.0324	-0.0883	-0,3620	-0.0054	0.3566	0.0102	-0.0104	0.0173
12	0.173 1.149	-0.01	37.5 -0.0219	-0.0846	-0,3448	-0.0100	0.3347	0.0255	-0.9872	0.0174
	0.176 1.199	0.01	37.5 -0.0060	-0.0004	-0.3653	-0.0086	0.3567	-0.0026	0.0472	0.0171
	0.157 0.949	2.00	37.5 -0.1589			0.0075	0.1781	0.0153	-0.0238	0.0171
-	0.163 1.000	2.00	37.5 -0.1744			0.0032	0.2108	0.0083	-0.0145	0.0174
-	0.167 1.052	2.00	37.5 -0.1772			0.0039	0.3440	0.0197	-0.0203	0.0182
-										-
17	0.170 1.100	2.00	37.5 -0.1841	-0.2782	-0,3578	-0.0053	0,3587	0.0101	-0.0067	0.0167
18	0,175 1,150	2.00	37.5 -0.1812	-0.2549	-0,3470	-0.0099	0.3432	0.0269	-0.1124	0.0180
19	0.178 1.200	2.00	37.5 -0.1672	-0,1787	-0,3694	-0.0074	0,3677	-0.0023	0.0384	0.0183
20	0.160 0.950	4.01	37.5 -2.2990	-0.3434	-0,1692	0.0064	0,1961	0.0243	-0.0837	0.0188
21	0.163 0.999	4.01	37.5 -0.3281	-0.4325	-0.1950	0.0035	0.2209	0.0191	-0.0556	0.0195
22	0.170 1.051	4.02	37.5 -0.3274	-0.3822	-0.3345	0.0118	0.3683	0.0090	-0.0122	0.0184
	0.173 1.100	4.01	37.5 -0.3353				0.3739		-0.0615	0.0193
	0.178 1.148	4.02	37.5 -0.3364				0.3534		-0.0983	0.0203
	0.183 1.199	4.02	37.5 -0.3227					-0.0011		0.0197
	0.160 0.949	6.02	37.5 -0.4587				0.2032		-0.1306	0.0232
	0.167 1.001	6.02	37.5 -0.4901				0.2558		-0.0872	0.0229
28	0.170 1.048	6.03	37.5 -0.4730	-0.4748	-0,3121	0.0084	0,3683		-0.0237	0.0206
29	0.175 1.099	6.03	37.5 -0.4984				0,4066		-0.0823	0.0227
30	0.178 1.150	6.03	37.5 -0.4952				Ø.3788		-0.1439	0.0236
33	0.168 1.198	6.03	37.5 -0.4783	-0.4584	-0,3796	-0.0096	0,4183	0.0054	0.0109	0.0219
34	0.150 0.952	8.03	37.5 -0.6202	-0.7240	-0.1523	0.0046	0.2420	0.0459	-0.1566	0.0263
	0.154 0.999		37.5 -8.6471	-0.7729	-0.1987		0.2895		-0.1531	0.0264
	0.158 1.048	8.04	37.5 -0.6686			0.0097	0.4240		-0.0855	0.0242
	0.163 1.099	-	37.5 -0.6655				0.4443		-0.1017	0.0251
-	0.167 1.149	-	37.5 -0.6689				0.4234		-0.2262	0.0238
•••	21207 21217	0.2	0.12		.,.,.					21.200
39	0.172 1.201	8.05	37.5 -0.6568				0.4766		-0.0127	0.0249
40	0.150 0.950	10.04	37.5 -0.8027	-0.9297	-0,1513	0.0014	0,2903	0.0695	-0.2063	0.0267
41	0.157 1.001	10.04	37.5 -0.8470	-0.9714	-0,1992	0.0023	0.3462	0.0638	-0.2218	0.0261
42	0.162 1.051	10.05	37.5 -0.8699	-0.9433	-0,3555	0.0102	0,5120	0.0474	-0.1499	0.0257
43	0.163 1.101	10.06	37.5 -0.8649	-0.9399	-0.3719	-0.0007	0.5166	0.0442	-0.1498	0.0263
44	0.168 1.150	10.06	37.5 -2.8658	-0.9357	-0,3578	-0.0121	0,4917	0.0671	-0.2532	0.0262

TABLE 1.12
DATE LISTINGS

## ROLL ANGLE = 37.5 DEG.

					0/1-	5-01			
SER	REYN MACH	THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F YAW M	ROLL M
	0.173 1.201	10.07	37.5 -0.8536				0.5225	0.0271 -0.0644	
46	0.152 0.949	12.05	37.5 -1.0169	-1.1728	-0,1564	0.0046	0.3699	0.0950 -0.3302	
47	0.158 1.000	12.07	37.5 -1.0591	-1.1837	-0,1987	0.0046	0.4202	0.0928 -0.3358	
48	0.162 1.049	12.07	37.5 -1.0859	-1.1689	-0.3470	0.0088	0,5752	0.0724 -0.2469	0.0255
49	0.168 1.102	12.07	37.5 -1.0878	-1.1752	-0,3792	-0.0073	0.5913	0.0778 -0.2575	0.0278
	0.168 1.148	12.08	37.5 -1.0857				0,5668	0.0983 -0.3864	
	0.173 1.198	12.10	37.5 -1.0743				0.5860	0.0488 -0.1687	
	0.155 0.951	14.07	37.5 -1.2494			0.0031	0.4376	0.1070 -0.4029	
54	0.158 0.999	14.08	37.5 -1.2964			0.0019	0,5014	0.1308 -0.4531	
55	0.162 1.049	14.09	37,5 -1.3249	-1.3793	-0,3403	0.0000	0,6527	0.1057 -0.3514	0.0267
	0.168 1.099	14.10	37.5 -1.5171				0.6683	0.1089 -0.3934	
	0.173 1.150	14.11	37.5 -1.3201				0.6601	0.1251 -0.4886	
	0.175 1.200	14.13	37.5 -1.3037				0,6882	0.0883 -0.3047	
59	0.155 0.951	16.08	37.5 -1.4896				0,5397	0.1308 -0.5026	
60	0.162 1.032	16.11	37.5 -1.5606	-1.6528	-0,1753	-0.0014	0.6001	0.1473 -0.5645	0.0220
61	0.165 1.049	16.12	37.5 -1.5815	-1.5529	-0,3445	0.0080	0.7779	0.1192 -0.4243	0.0259
62	0.158 1.099	16.13	37.5 -1.2623	-1,5077	-0,3751	-0.0096	0.7852	0.1424 -0.5186	0.0329
63	0.173 1.149	16.14	37.5 -1.5667				0.7660	0.1471 -0.5824	0.0306
64	0.176 1.199	16.16	37.5 -1.5674	-1.1470	-0,3917	-0.0152	0.7982	0.1167 -0.4019	0.0353
67	0.147 0.949	18.10	37.5 -1.7469	-1.9367	-0,1212	-0.0015	0,6565	0.1652 -0.5924	0.0333
63	0.152 0.998	18.12	37.5 -1.8527	-1.9417	-0.1548	-0.0038	0.7197	Ø.1821 -Ø.6686	0.0268
69	0.155 1.046	18.15	37.5 -1.8448	-1.5937	-0.3220	0.0019	0.8824	0.1500 -0.5239	0.0333
72	0.157 1.049	18.15	37.5 -1.8617	-1.6511	-0,3263	0.0003	0.8902	0.1507 -0.5238	0.0330
71	0.162 1.098	18.16	37.5 -1.8551	-1.6507	-0,3565	-0.0144	0.9031	0.1474 -0.5809	0.0388
72	0.167 1.151	18.17	37.5 -1.8802				0.9130	0.1798 -0.6940	0.0361
73	0.168 1.202	18.21	37.5 -1.9283	-1.2347	-0,3890	-0.0150	0.9578	0.1363 -0.5075	0.0425
74	0.150 0.949	20.13	37.5 -2.0896	-2.1849	-0,1133	-0.0076	0.8184	0.1886 -0.6511	0.0450
75	0.154 0.998	47.06	37.5 -2.2174				0.9032	0.1821 -0.5650	0.0365
76	0.157 1.049	20.19	37.5 -2.2618	-1.8772	-0.3457	-0.0013	1.1038	0.1588 -0.5524	0.0423
	0.163 1.099	20.20	37.5 -2.2589				1.1013	0.1794 -0.6681	0.0491
78	0.167 1.149	20.23	37.5 -2.2925	-1.6554	-0.3553	-0.0193	1.1080	0.1787 -0.6730	0.0443
	0.168 1.200	20.27	37.5 -2.3537				1.1549	0.1235 -0.4726	
	0.150 0.951	22.17	37.5 -2.4711				1.0279	0.1831 -0.6515	
	0.154 0.999	22.23	37.5 -2.6869				1.1456	0.1917 -0.7064	
	0.160 1.049	22.25	37.5 -2.7129				1.3250	0.1514 -0.5296	
	0.163 1.100	22.26	37.5 -2.7195				1.3298	0.1793 -0.6020	
	0.168 1.150	22.29	37.5 -2.7719				1.3532	0.1743 -0.6335	
	0.172 1.200	22.34	37.5 -2.8239				1.4020	0.0972 -0.3915	
	0.152 0.953	24.24	37.5 -2.9387				1.2691	0.2014 -0.7100	
87	0.157 1.000	24.30	37.5 -3.1819	-2.0552	-0,1529	-0.0121	1.4376	0.2253 -0.7676	0.0465
88	0.163 1.049	24.32	37.5 -3.2410	-2.0351	-0,3223	-0.0096	1.6199	0.1691 -0.5552	0.0508

TABLE 1.12

## ROLL ANGLE = 37,5 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F YAW M	ROLL M
89	0.165	1.171	24.32	37.5	-3.2343	-2.1183	-0,3298	-0.0258	1.6097	0.1560 -0.5771	0.0563
90	0.168	1.151	24.38	37.5	-5.2954	-1.8302	-0,3153	-0.0271	1.6227	0.1833 -0.6257	0.0494
91	0.173	1.200	24.42	37.5	-3.3653	-1.5254	-0,3638	-0.0225	1.7022	0.1461 -0.4747	0.0562
92	0.155	0.952	26.31	37.5	-3.4057	-2.0798	-0.0606	-0.0162	1.5495	0.2092 -0.7310	0.0746
93	0.158	0.998	26.36	37.5	-3.6666	-2,0482	-0.1130	-0.0137	1.7174	0.2092 -0.7892	0.0584
94	0.163	1.049	26.40	37.5	-3.7586	-2,0998	-0,3228	-0.0168	1,9452	0.1649 -0.5982	0.0575
95	0.168	1,121	26.41	37.5	-3.7953	-2.2527	-0.3239	-0.0318	1.9499	0.1618 -0.5717	0.0574
96	0.172	1.148	26.45	37.5	-3.8429	-1.9989	-0,3122	-0.0301	1.9636	0.1541 -0.5950	0.0545
97	0.176	1.199	26.50	37.5	-3.9018	-1.6813	-0,3382	-0.0248	2.0216	0.1497 -0.4519	0.0516
98	0.155	0.949	28.38	37.5	-3.9046	-1.9935	-0,0367	-0.0171	1.8735	0.1980 -0.6970	0.0809
99	Ø.162	1.001	28.45	37.5	-4.1665	-1,8432	-0,0930	-0.0161	2,0527	0.2431 -0.8210	0.0624
100	0.165	1.048	28.47	37.5	-4.2983	-2.1334	-0,2940	-0.0154	2.2905	0.1761 -0.6022	0.0566
101	0.168	1.120	28.49	37.5	-4.3375	-2.3287	-0,3133	-0.0307	2.3177	0.1544 -0.5638	0.0584
102	0.173	1.148	28.53	37.5	-4.3896	-2,1209	-0,2811	-0.0337	2.3144	0.2249 -0.7446	0.0563
103	0.176	1.198	28.59	37.5	-4.4539	-1,8855	-0,3197	-0.0275	2.3876	0.1580 -0.4658	0.0537

TABLE 1.13

POLL	ANGLE	= 45	DEG.

SER	REYN MACH	THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
	0 444 0 054		45 0 7 4440	a anna	-0 1515	0.0080	4 4 4 7 5	0 0004	-0 0474	0 0407
CT	0.144 0.951	-2.02	45.0 0.1162	-	-0,1515		0.1635		-0.0134	0.0183
	0.149 0.998	-2.02	45.0 0.1267		-0,1882	0.0065	0.1990		-0.0167	0.0183
-	0.155 1.051	-2.02	45.0 7.1148		-0,3300	0.0133	0.3471		-0.0194	0.0182
	0.158 1.099	-2.02	45.0 0.1262		-0.3593		0.3559		-0.0342	0.0185
110	0.162 1.149	-2.02	45.0 0.1330	0.10/5	-0.3407	-0.0090	0,3362	0.0252	-0.0907	0.0182
111	0.163 1.199	-2.02	45.0 0.1527	0.1758	-0,3627	-0.0081	0.3597	-0.0023	0.0550	0.0174
112	0.147 0.951	0.01	45.0 -0.0180	-0.0327	-0,1451	0.0079	0.1530	0.0190	-0.0271	0.0175
113	0.152 0.999	0.01	45.0 -0.0260	-0,0530	-0,1948	0.0064	0.2012	0.0235	-0.0450	0.0174
114	0.155 1.050	0.01	45.0 -1.0288	-0.0684	-0,3456	0.0122	0.3578	0.0113	-0.0158	0.0173
115	0.160 1.101	0.01	45.0 -0.0192	-0.0617	-0.3614	-0.0062	0.3552	0.0172	-0.0171	0.0178
116	0.163 1.148	-0.01	45.0 -0.0246	-0.0677	-0.3416	-0.0077	0.3339	0.0286	-0.0843	0.0180
117	0.167 1.200	0.01	45.0 -0.0033	0.0032	-0.3700	-0.0066	0.3634	-0.0037	0.0241	0.0171
118	0.147 0.951	2.01	45.0 -0.1564	-0.1802	-0,1699	0.0067	0.1819	0.0147	-0.0275	0.0179
	0.154 0.998	2.00	45.0 -0.1725			0.0074	0.2168	0.0142	-0.0361	0.0172
120	0.157 1.050	2.01	45.0 -0.1767	-0.2277	-0.3300	0.0118	0.3477	0.0063	-0.0016	0.0179
121	0.160 1.099	2.01	45.0 -0.1840	-0.2711	-0.3470	0.0048	0.3580	0.0129	-0.0291	0.0183
122	0.167 1.151	2.00	45.0 -0.1815	-0.2460	-0.3470	-0.0088	0.3443	0.0186	-0.2846	0.0189
123	0.167 1.199	2.01	45.0 -0.1616	-0.1644	-0.3724	-0.0074	0.3704	-0.0063	0.0596	0.0183
124	0.150 0.949	4.01	45.0 -0.2980	-0.3388	-Ø,1582	0.0067	0.1853	0.0150	-0.0342	0.0189
125	0.154 0.998	4.00	45.0 -0.3280	-0.4201	-0,1959	0.0046	0.2230	0.0108	-0.0186	0.0193
124	0.157 1.049	4.02	45.0 -0.3145	-0 3271	-0 3145	0.0088	0.3465	0 0138	-0.0085	0.0184
	0.163 1.101	4.02	45.0 -0.3340				0.3705		-0.0320	0.0193
	0.167 1.150	4.01	45.0 -0.5311				0.3520		-0.0833	0.0196
	0.172 1.200	4.02	45.0 -0.3200					-0.0134		0.0191
	Ø.152 Ø.952	6.02	45.0 -0.4487				0.2017		-0.0274	0.0218
130	D.1172 D.1772	0.02	45,6 -014407	0,0004	511210	D. D. D. T.	D. Z.D. 1.	D. D. L. Z. C	-0102/4	0.0210
131	0.157 1.001	6.02	45.0 -0.4801	-0.5925	-0,1900	0.0029	0.2423	0.0115	-0.0371	0.0215
132	0.160 1.049	6.03	45.0 -0.4836	-0.5192	-0,3232	0.0119	0.3840	0.0035	0.0090	0.0218
133	0.163 1.099	6.03	45.0 -0.4953	-Ø.5778	-0,3611	-0.0039	0.4072	0.0115	-0.0254	0.0227
134	0.167 1.148	6.03	45.0 -0.4950	-0.5544	-0,3323	-0.0093	0.3732	0.0171	-0.0798	0.0234
135	0.172 1.199	6.04	45.0 -0.4784	-0.4561	-0,3742	-0.0095	0.4130	-0.0148	0.0601	0.0224
138	0.145 0.950	8.03	45.0 -0.6091	-0.6729	-0.1552	0.0062	0.2449	0.0228	-0.0338	0.0247
- CONTRACTOR - CON	0.149 1.001	8.03	45.0 -0.6473			0.0020	0.2932	0.0049		0.0256
	0.152 1.050	8.04	45.0 -0.6629			0.0104	0.4380	0.0035	0.0449	0.0270
_	0.157 1.099	8.05	45.0 -0.6610				0.4475	-0.0057	0.0318	0.0267
	0.158 1.149	8.04	45.0 -0.6631				0.4190		-0.0861	0.0263
	01170 11147	0.04	1515 515031		D ( 0 4 D 0	0.020	2,1270	0,020,	0,10001	012200
143	0.165 1.198	8.05	45.0 -0.6476	-0.5583	-0,3847	-0.0102	0.4616	-0.0151	0.0815	0.0270
144	0.147 0.952	10.04	45.0 -0.1998	-0.8928	-0.1443	0.0007	0.2823	0.0101	-0.0064	0.0275
145	0.149 0.999	10.05	45.0 -0.8340	-0.9546	-0,1908	0.0003	0.3336	0.0049	0.2004	0.0290
146	0.155 1.052	10.05	45.4 -0.8523	-0.8925	-0,3351	0.0016	0.4803	0.0046	0.0293	0.0289
147	0.158 1.101	10.05	45.0 -0.8545	-0.9143	-0,3739	-0.0047	0.5127	0.0001	0.0272	0.0295
148	0.163 1.151	10.06	45.0 -0.8599	-0.9130	-0,3539	-0.0140	0.4849	0.0241	-0.0827	0.0285

TABLE 1.13

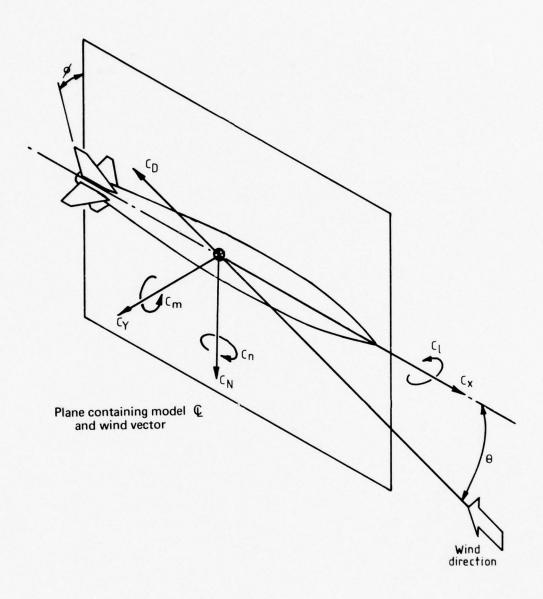
ROLL ANGLE = 45 DEG.

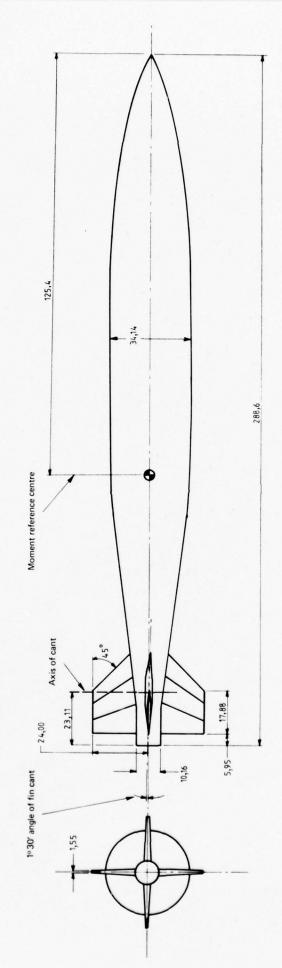
SER	REYN MACH	THETA	RANG NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
140	0.165 1.198	10.07	45.0 -0.8422	-0.7426	-0.3892	-0.0133	0.5174	-0.0152	0.0888	0.0282
	0.147 0.951		45.0 -1.0076			0.0035	0.3474	0.0239		0.0282
	0.152 0.999		45.4 -1.0481			0.0006	0.4088	0.0286	0.0028	0.0273
	0.155 1.050		45.4 -1.0778			0.0086	0.5692	0.0055	0.0160	0.0279
- TO 100 100	0.160 1.131		45.6 -1.0715			-0.0083	0.5885	0.0045	0.0243	0.0308
	0.163 1.149		45.0 -1.0769				0.5624	0.0319		0.0283
	0.167 1.198		45.0 -1.0665				0.5902	-0.0066		0.0274
	0.145 0.950		45,0 -1.2294			0.0062	0.4325	0.0339	200 Table 100 Co.	0.0191
-	0.149 1.032		45.0 -1.2666			0.0020	0.4994	0.0219		0.0198
160	0.152 1.050	14.09	45,6 -1.3126	-1.3525	-0,3355	0.0099	0.6545	0.0228	-0.0260	0.0193
144	0.157 1.099	14.09	45.0 -1.3005	-1 3081	-0 3458	0.0009	0.6724	0.0199	-0 3106	0.0241
	0.158 1.152		45.0 -1.3027				0.6509	0.0366		0.0239
	0.162 1.199		45.0 -1.2810				Ø.6789	0.0024		0.0216
-	0.145 0.949		45.0 -1.4659			The second second	0.5207	0.0527		0.0100
-	0.149 0.998		45.0 -1.5300				Ø.5828	0.0462		0.0096
•••	•••				-,					
166	0.152 1.048	16.12	45.0 -1.5454	-1.4277	-0.3233	0.0029	0.7424	0.0566	-0.1141	0.0070
167	0.158 1.100		45.0 -1.5517	-1.4612	-0.3642	-0.0113	0.7699	0.0390	-0.0874	0.0192
168	0.158 1.148	16.14	45.0 -1.5550				0.7562	0.0524	-0.1818	0.0174
169	0.165 1.198	16.16	45.0 -1.5597	-1.0947	-0.3942	-0.0148	0.7986	0.0134	-0.0013	0.0214
170	0.145 0.950	18.10	45.0 -1.7408	-1.8864	-Ø,1378	-0.0055	0.6668	0.0617	-0.1704	0.0120
_										
	0.152 1.001		45.0 -1.8277				0.7349	0.0753		0.0055
	0.155 1.049		45.0 -1.8544				0.8953	0.0674		0.0062
	0.158 1.098		45.0 -1.8501				0.9072	0.0599		0.0220
- T. C. C. C. C.	Ø.162 1.147		45.0 -1.8774				0,9068	0.0615		0.0190
1/5	0.167 1.199	18.21	45.0 -1.9077	-1.1584	-0,3891	-0.0155	0,9511	0.0308	-0.0000	0.0217
176	0.147 0.952	20.14	45.0 -2.0736	-2.0777	-0.1127	-0.0065	0.8137	0.0675	-0.1850	0.0133
	0.152 1.001		45.0 -2.2053				0.9081	0.0941	The second second	0.0047
	0.155 1.053		45.0 -2.2711	-1.9073	-0.3629	-0.0007	1.1240	0.0779		0.0104
179	0.160 1.101		45.0 -2.2384				1.0965	0.0672	-0.1802	0.0258
180	0.163 1.151	20.23	45.0 -2.2845				1.0929	0.0684	-0.2482	0.0234
	0.167 1.200		45.0 -2.3369				1.1485	0.0453		0.0243
	0.147 0.949		45.0 -2.4513				1.0089	0.0752		0.0130
	0.154 1.000		45.0 -2.6598				1.1310	0.0974		0.0053
	0.160 1.049		45.0 -2.7005				1.3055	0.1258		0.0072
187	0.163 1.099	22.26	45.0 -2.6768	-1.9028	-0,3476	-0.0167	1.3202	0.0776	-0.1967	0.0262
100	0.167 1.150	20 30	45.0 -2.7431	-1 6414	-0 3447	-0.0249	1.3387	0.0810	-0 2420	0.0242
	0.172 1.220		45.0 -2.7922				1.3879	0.0325		0.0265
-	0.152 0.950		45.0 -2.9205				1.2536	0.0525		0.0133
	0.157 0.999		45.0 -3.1765				1.4171	0.0834		0.0050
	0.160 1.052		45.0 -3.2264				1.6110	0.1013		0.0055
		24.00			2,0200			3.1510		
197	0.165 1.101	24.34	45.0 -3.2186	-2.0102	-0,3402	-0.0249	1.6140	0.0785	-0.2169	0.0227

TABLE 1.13
DATA LISTINGS

## ROLL ANGLE = 45 DEG.

SER	REYN	MACH	THETA	RANG	NORMAL	PITCH	AXIAL	BASE	DRAG	SIDE F	YAW M	ROLL M
194	0.168	1.148	24.37	45.0	-3.2769	-1.7917	-0,3247	-0.0282	1.6228	0.0581	-0.2007	0.0229
195	0.172	1.198	24.42	45.0	-3.3267	-1.4655	-0,3579	-0.0228	1.6808	0.0548	-0.1044	0.0210
196	0.152	0.949	26.32	45.0	-3.3566	-1.8634	-0,0637	-0.0129	1.5339	0.0511	-0.1367	0.0122
197	0.157	1.001	26.38	45.0	-3.6634	-1.8940	-0.1255	-0.0092	1.7321	0.0790	-0.1701	0.0046
198	0.160	1.048	26.41	45.0	-3.7110	-1.8630	-0,2951	-0.0128	1,9035	0.0884	-0.2135	0.0050
199	0.165	1.099	26.42	45.0	-3./834	-2.1223	-0,3127	-0.0206	1,9453	0.0742	-0.2066	0.0167
200	0.168	1,148	26.46	45,0	-3.8327	-1.9078	-0.3062	-0.0286	1,9555	0.0860	-0.2140	0.0161
201	0.173	1.199	26.51	45.0	-3.8898	-1.5961	-0,3358	-0.0243	2.0152	0.0860	-0.1517	0.0186
202	0.152	0.950	28.39	45.0	-3.8410	-1.7773	-0.0244	-0.0142	1.8355	0.0791	-0.1860	0.0191
203	0.158	1.001	28.46	45.0	-4.1559	-1.7617	-0,1023	-0.0130	2.0591	0.1128	-0.2128	0.0054
204	0.162	1.052	28.47	45.0	-4.2822	-2.0868	-0,3052	-0.0121	2,2999	0.1243	-0.2619	0.0048
205	0.165	1.102	28.49	45.0	-4.3131	-2.2470	-0,2980	-0.0277	2,2956	0.1085	-0.2642	0.0140
206	0.172	1.149	28.54	45,0	-4.3687	-2.0341	-0,2934	-0.0337	2.3157	0.1145	-0.2893	0.0136
207	0.173	1.271	28.59				-0,3105		2.3713	0.0733	-0.1181	0.0128





All dimensions in millimetres

FIG. 2 1/8 SCALE MODEL MK 82 BOMB

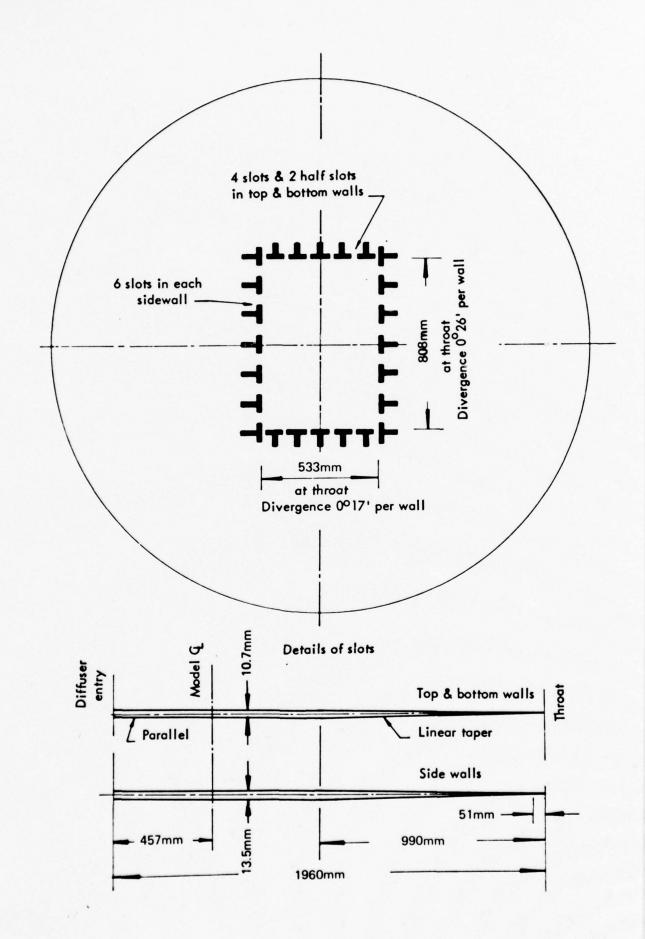
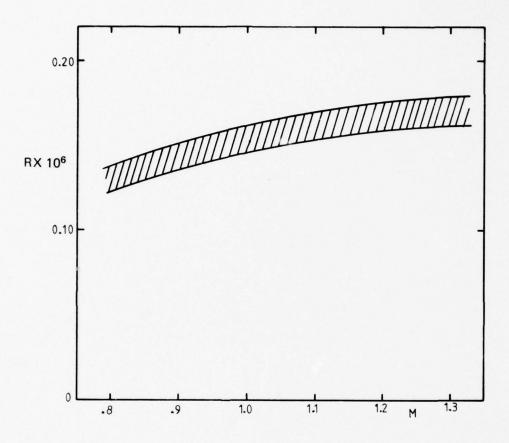


FIG. 3 DETAILS OF SLOTTED TEST SECTION



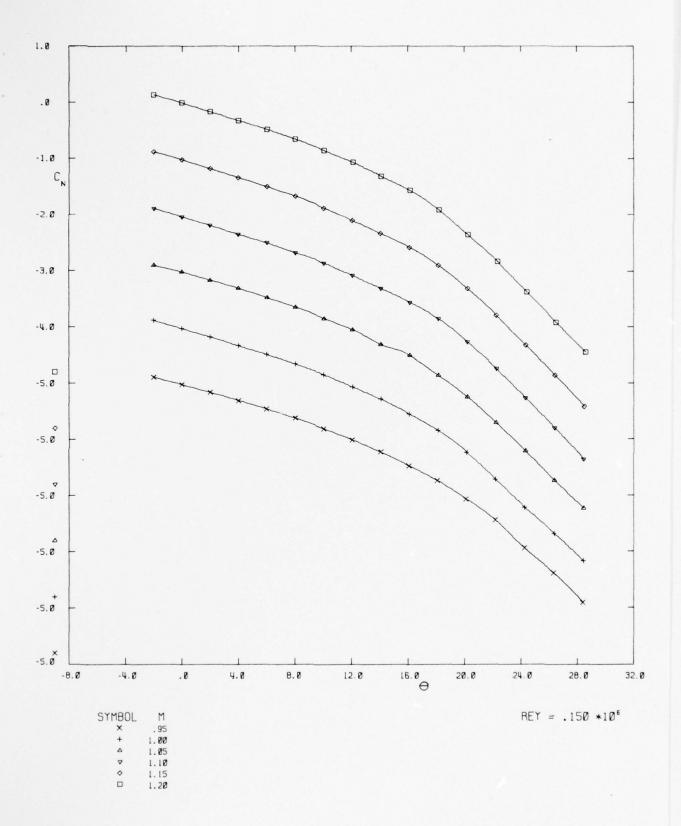


FIG. 5a VARIATION OF NORMAL FORCE COEFFICIENT WITH THETA ROLL ANGLE = -45 DEG.

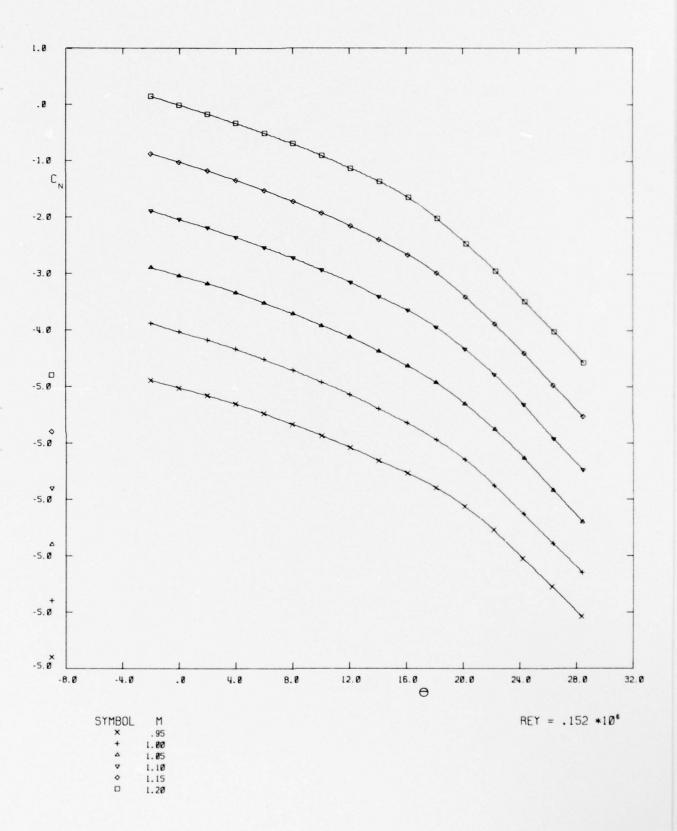


FIG. 5b VARIATION OF NORMAL FORCE COEFFICIENT WITH THETA ROLL ANGLE =  $\cdot 22.5$  DEG.

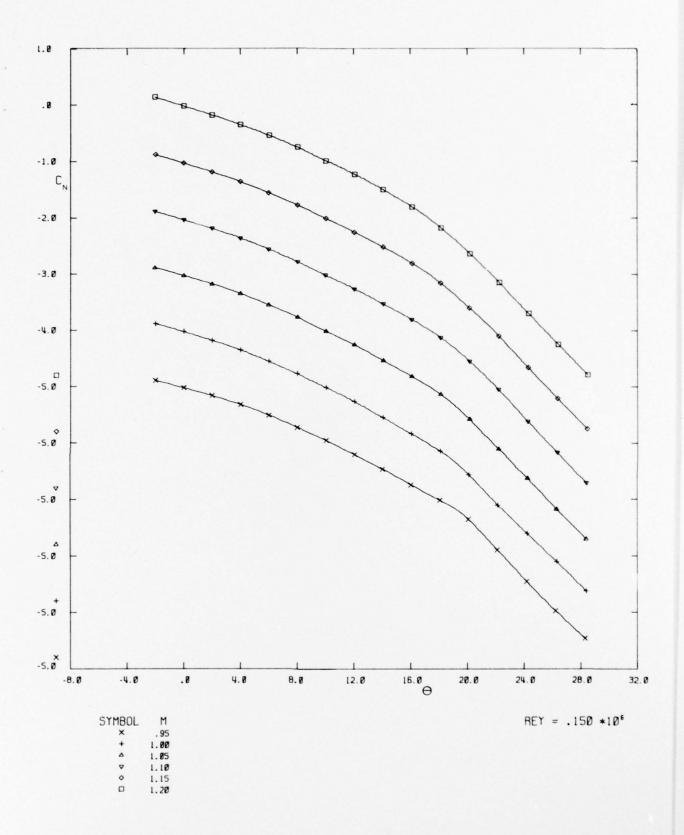


FIG. 5c VARIATION OF NORMAL FORCE COEFFICIENT WITH THETA ROLL ANGLE = 0 DEG.

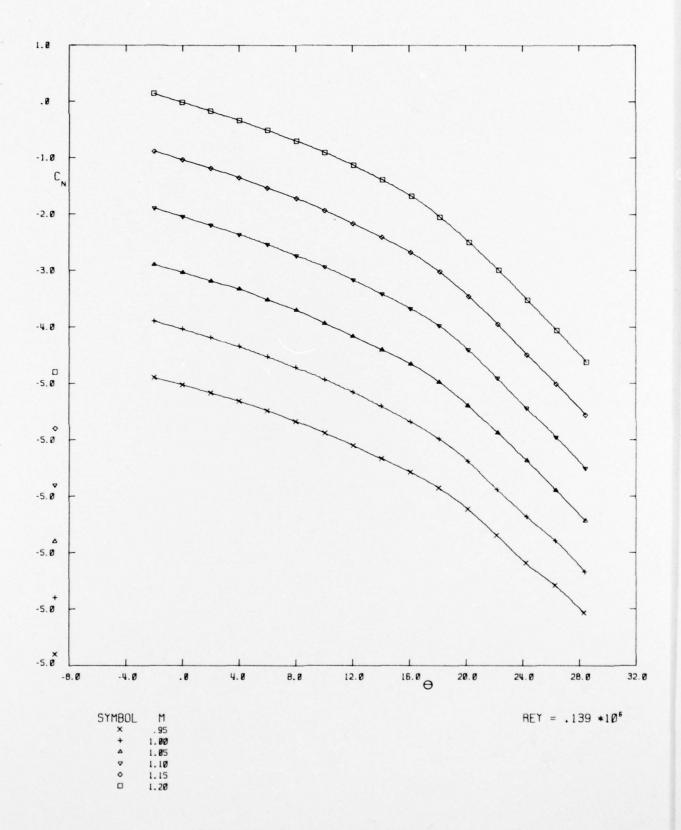


FIG. 5d VARIATION OF NORMAL FORCE COEFFICIENT WITH THETA ROLL ANGLE = 22.5 DEG.

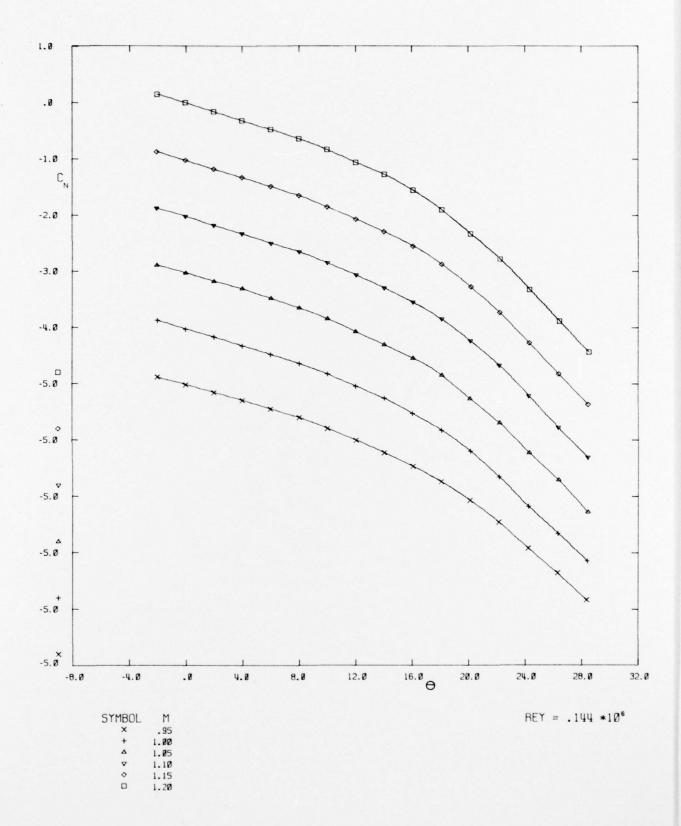
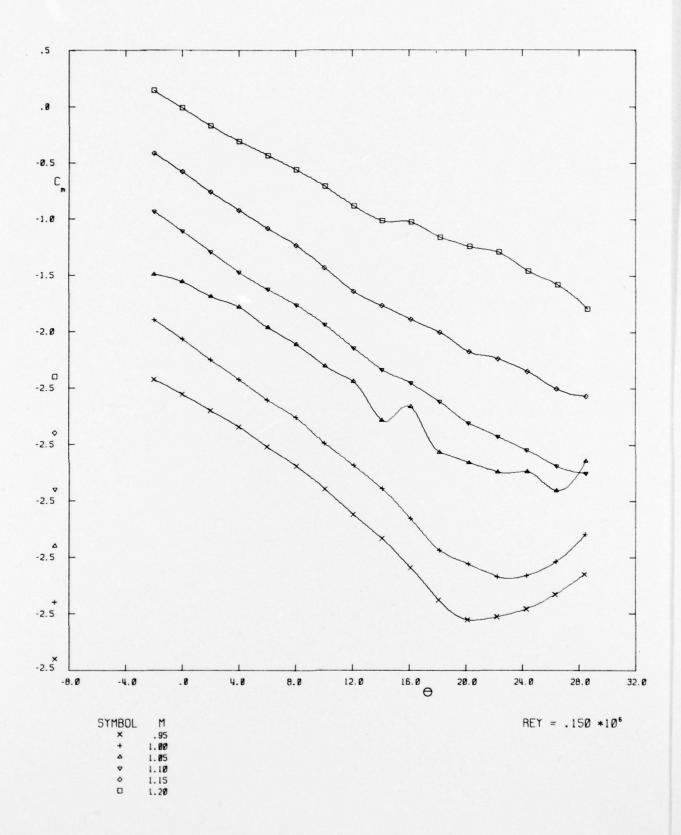
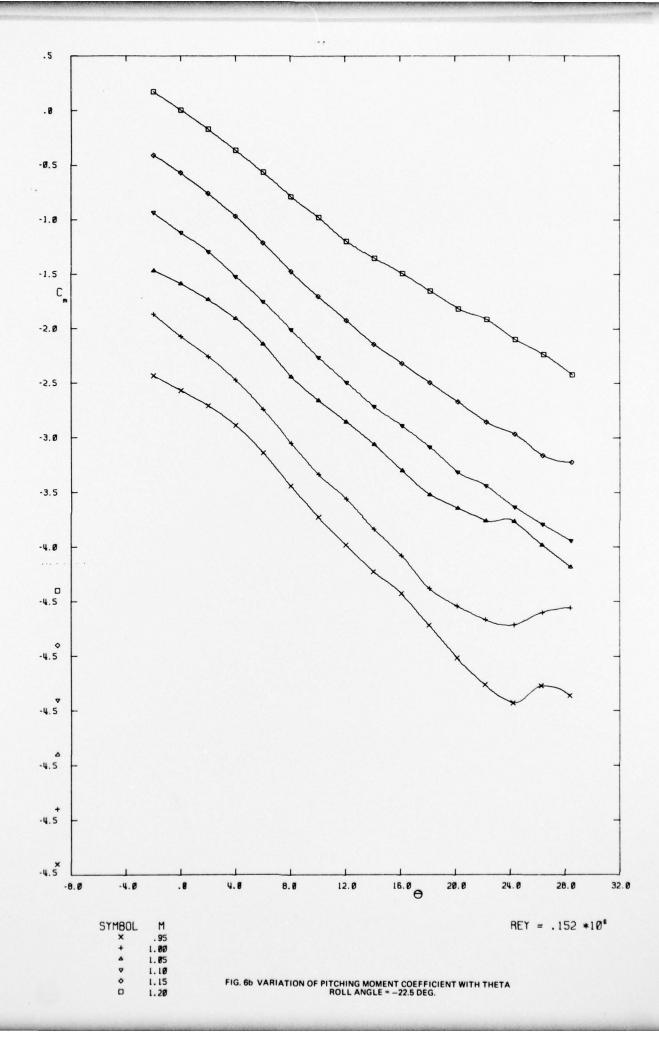
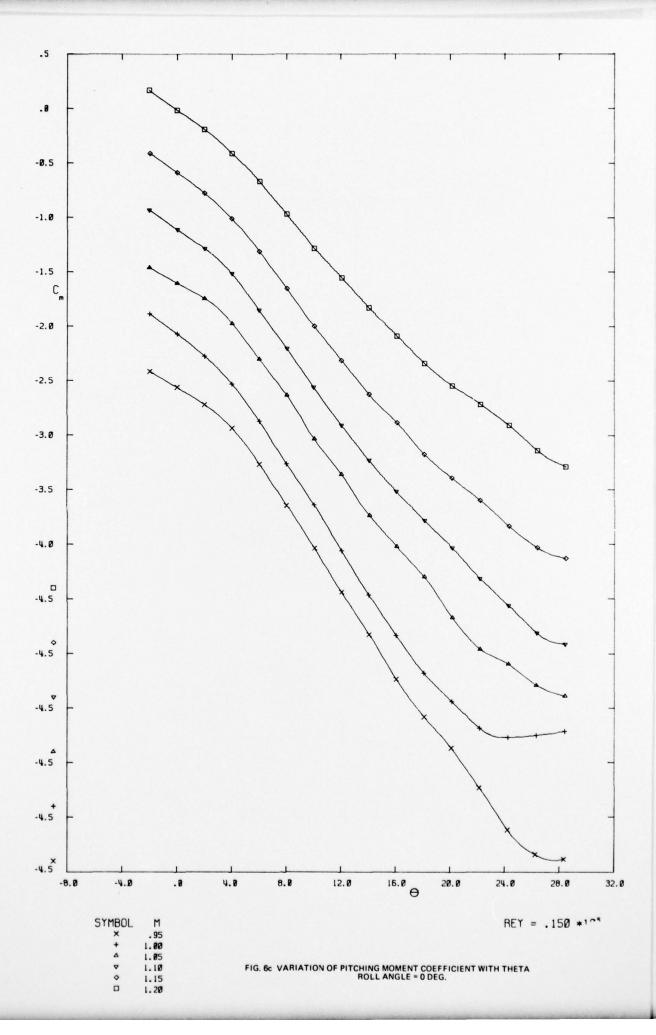
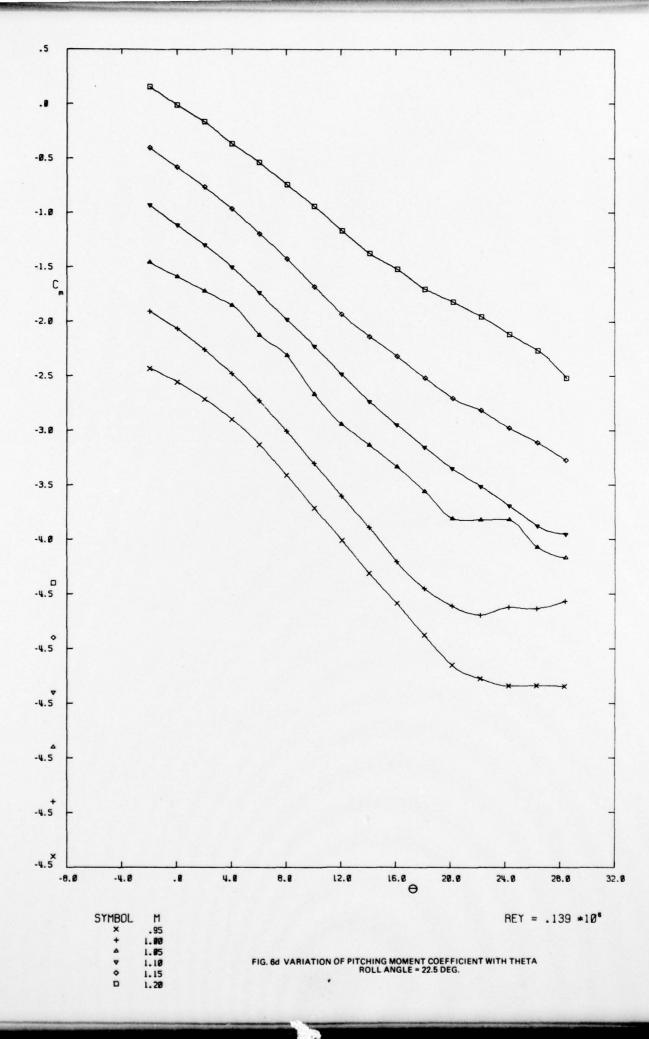


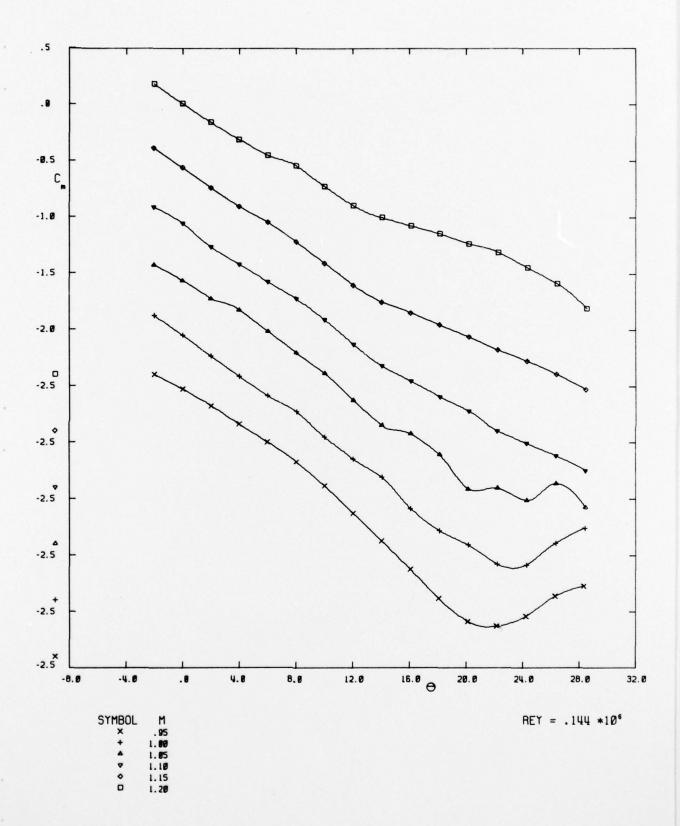
FIG. 5e VARIATION OF NORMAL FORCE COEFFICIENT WITH THETA ROLL ANGLE = 45 DEG.











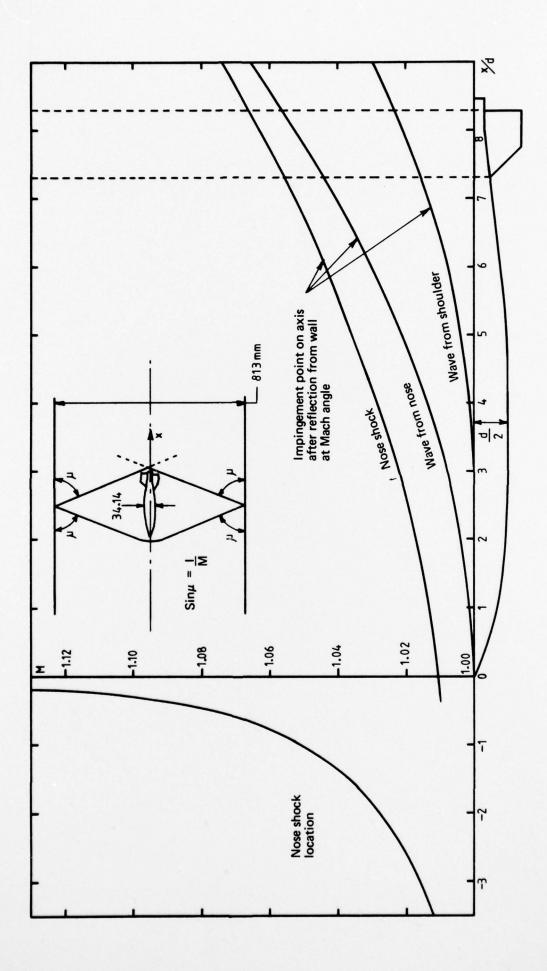
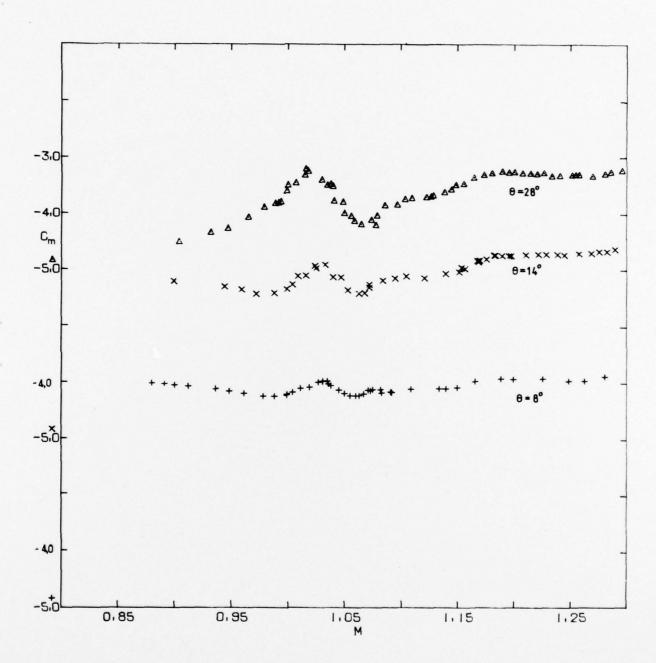


FIG. 7 MACH NUMBER RANGE OF WALL-REFLECTED WAVE INTERFERENCE



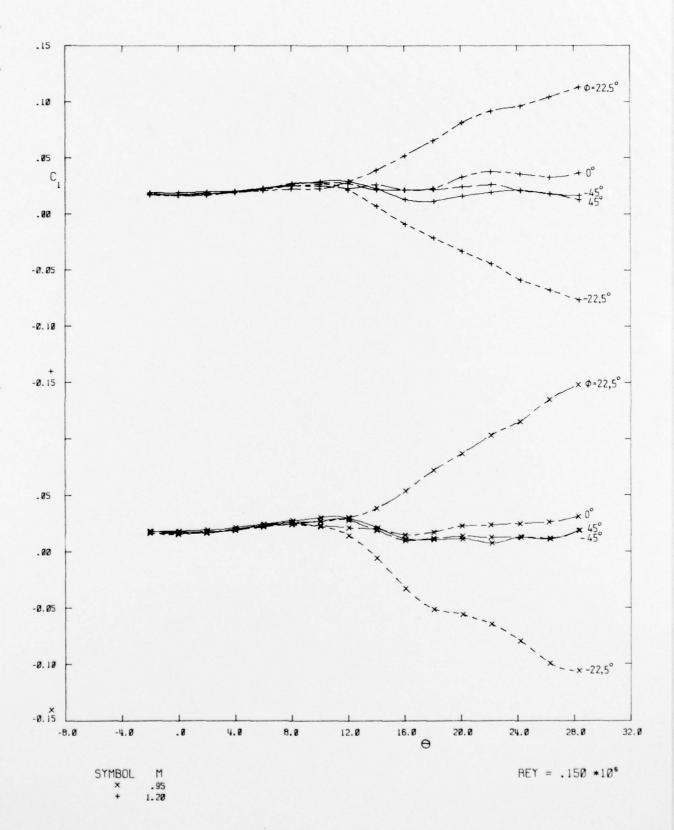


FIG. 9 VARIATION OF ROLLING MOMENT COEFFICIENT WITH THETA EFFECT OF ROLL ANGLE

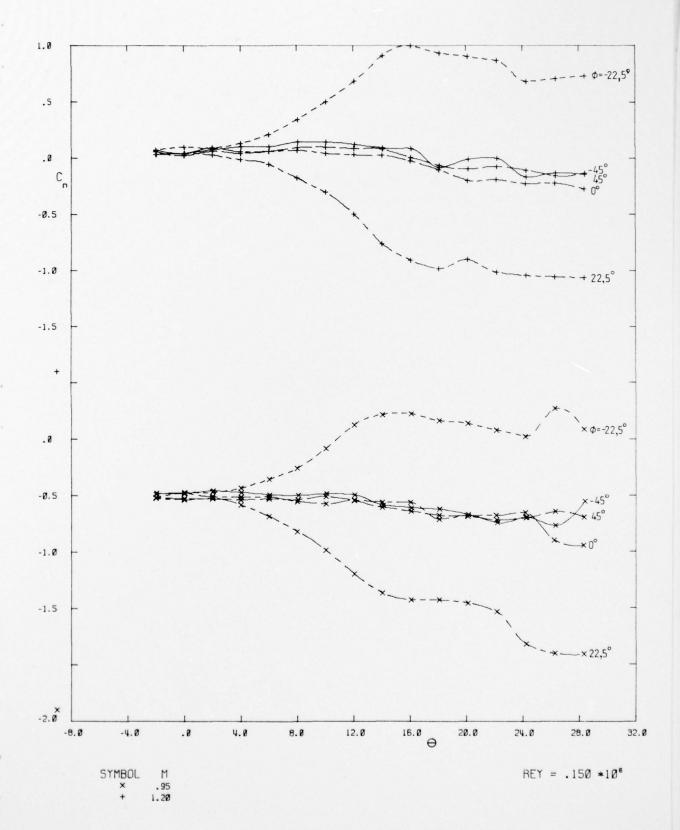


FIG. 10 VARIATION OF YAWING MOMENT COEFFICIENT WITH THETA EFFECT OF ROLL ANGLE

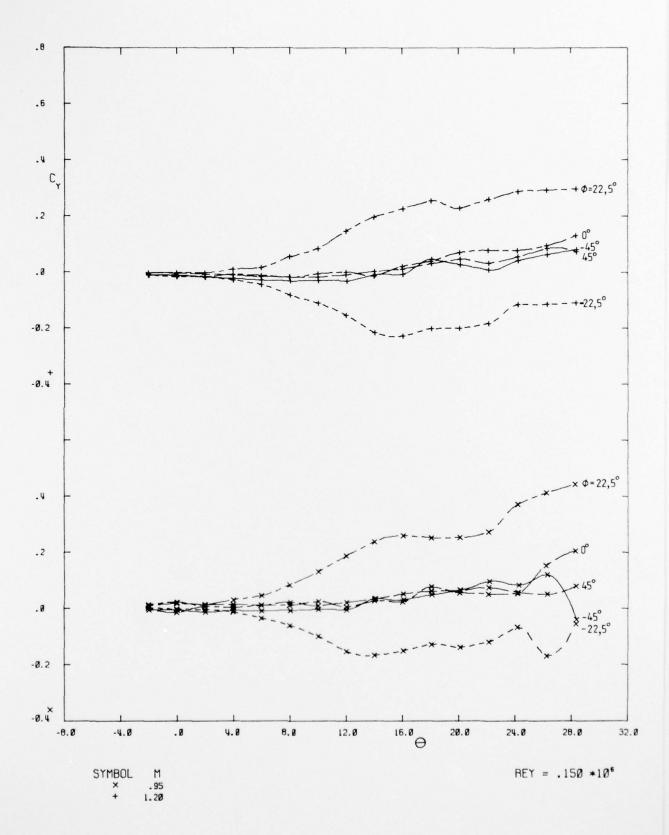


FIG. 11 VARIATION OF SIDE FORCE COEFFICIENT WITH THETA EFFECT OF ROLL ANGLE

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